

STAGE1: THE DIFFERENTIAL PAIR

The first stage in this audio amplifier is the differential-pair circuit of Figure P7-2.

a) DC BIAS

Determine values for the resistances R_{1A} , R_{1B} , and R_2 to achieve the following bias voltages and currents (assume $\beta = 100$ for each transistor). HINTS: Apply superposition and symmetry.

- $I_{BIAS} \approx 500\mu A$
- $V_{O1} = V_{O2} \approx 9.3V$

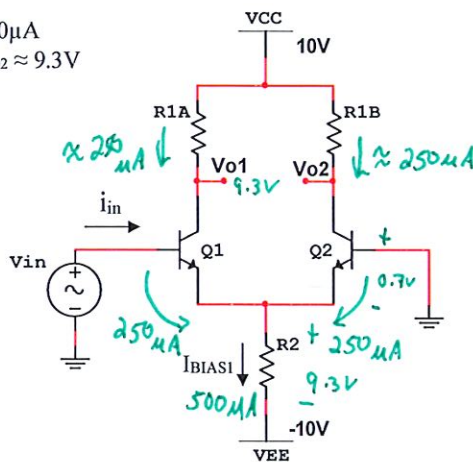


Figure P7-2

b) SMALL SIGNAL ANALYSIS

Now using small-signal analysis find the following:

- Small-signal voltage gains v_{O1}/v_{in} and v_{O2}/v_{in} .
- Differential output gain $(v_{O1}-v_{O2})/v_{in}$.
- Small-signal input resistance R_{in} at the input to the amplifier.

NOTE: In this example, since one of the inputs is tied to ground, the bias current I_{BIAS1} will remain fairly constant. Therefore, it may be set to zero in the small-signal model. Also, since only one single-ended output is required to drive the next stage, one of the collector resistors may be replaced with a short circuit without affecting the performance of this amplifier.

c) SIMULATION

Produce graphs of $v_{O1}(t)$, $v_{O2}(t)$ and for $v_{O1}(t) - v_{O2}(t)$ for an input signal of v_{in} being a 10mVpk 1kHz sine wave signal. NOTE: Expect only a small fluctuation in the output (less than a volt). Use the 2N3904 NPN BJT model for simulation.

DC BIAS

$$R_2 = \frac{-0.7V - (-10V)}{500\mu A}$$

$$= \frac{9.3V}{500\mu A} = 18.6K\Omega$$

$$\approx \boxed{20K\Omega (KIT)}$$

$$R_{1A} = R_{1B} = \frac{10V - 9.3V}{250\mu A}$$

$$= \frac{0.7V}{250\mu A} = 2.8K\Omega$$

$$\approx \boxed{3K (KIT)}$$

SMALL-SIGNAL

$$\frac{v_{O1}}{v_{in}} = \frac{-R_c}{r_e + r_e || R_E} \approx -\frac{R_c}{2r_e}$$

$$g_m = \frac{I_c (BIAS)}{mV_T} = \frac{250\mu A}{(17)(25mV)}$$

$$= 10mA/V$$

$$r_e = \left(\frac{\beta}{\beta+1}\right) \left(\frac{1}{g_m}\right) \approx \underline{\underline{100\Omega}}$$

$$\therefore \frac{v_{O1}}{v_{in}} = -\frac{3K}{2(100\Omega)} = \boxed{-15V/V}$$

$$\frac{v_{O2}}{v_{in}} = +\frac{3K}{2(100\Omega)} = \boxed{+15V/V}$$

$$\therefore \frac{v_{O1}-v_{O2}}{v_{in}} = \boxed{-30V/V}$$

STAGE 2: COMMON EMITTER BJT AMPLIFIER WITH ACTIVE LOAD

The output of the differential pair is then connected to a Common Emitter BJT Amplifier comprised of a PNP transistor with an active (current source) load as shown in Figure P7-3. This configuration relies on the high input impedance of the current source to achieve high gain.

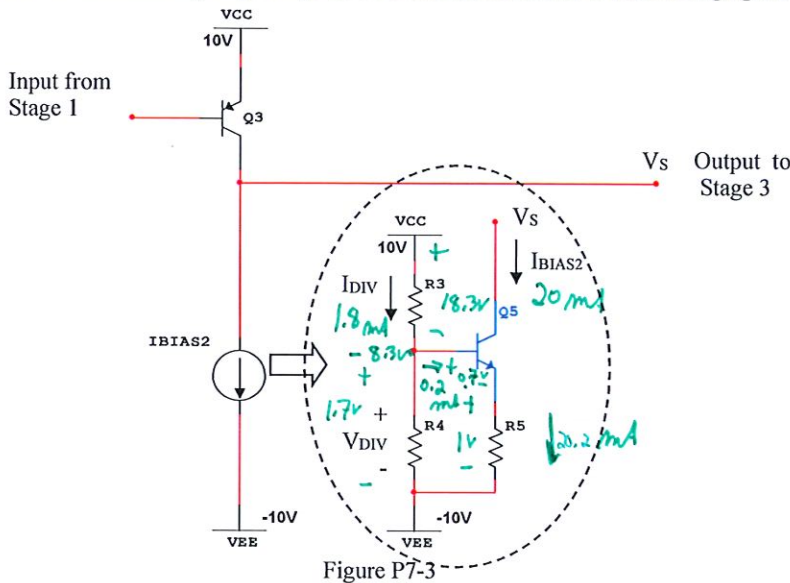


Figure P7-3

a) DC CURRENT SOURCE DESIGN

The actual current source circuit is comprised of a NPN BJT and a voltage divider network (oval insert). Choose values for the resistors R3, R4 and R5 to achieve the following specifications (assuming $\beta = 100$):

- $I_{BIAS2} \approx 20mA$
- $I_{DIV} \approx 1.8mA$ (with Q5 disconnected)
- $V_{DIV} \approx 1.7V$ across R4

b) SIMULATION

- Using DC ANALYSIS in simulation, verify the values of I_{BIAS2} , I_{DIV} and V_{DIV} .
- Connect the output of the current source to a separate DC supply (V_s) and use DC SWEEP analysis to vary the voltage from -10 to +10 Volts.
- Produce a plot of I_{BIAS2} as a function of V_s . What is the dynamic voltage range of the output? (ie. Over what range of output voltage does the current source work properly?)

$$I_C = 20mA \quad \left. \begin{array}{l} \\ \\ \end{array} \right\} I_E = 20.2mA$$

$$I_B = 200\mu A$$

$$R_5 = \frac{1V}{20.2mA} = 49.5\Omega$$

$$\approx \boxed{51\Omega (KIT)}$$

$$R_3 = \frac{10V - (-8.3V)}{1.8mA} = \frac{18.3V}{1.8mA}$$

$$= 10.17K\Omega$$

$$\approx \boxed{10K\Omega (KIT)}$$

$$R_4 = \frac{1.7V}{1.8mA - 0.2mA} = 1.06K\Omega$$

$$\approx \boxed{1K (KIT)}$$

(OR)

$$R_4 = \frac{1.7V}{1.8mA} = 944\Omega$$

w/ Q5 DISCONNECTED