

19.1 (a) For a homogeneously broadened system, the gain is reduced by a factor of two when the signal intensity equals the saturation intensity, given by

$$I_s = \frac{h\nu}{\sigma\tau_2} = \frac{hc}{\lambda\sigma\tau_2} = \frac{(6.63 \times 10^{-34})(3 \times 10^8)}{(5.5 \times 10^{-7})(4 \times 10^{-20})(3 \times 10^{-9})} = 3.01 \times 10^9 \text{ W/m}^2$$

(b) For Nd:glass, the saturation intensity is

$$I_s = \frac{(6.63 \times 10^{-34})(3 \times 10^8)}{(1.054 \times 10^{-6})(4 \times 10^{-24})(290 \times 10^{-6})} = 1.63 \times 10^8 \text{ W/m}^2$$

If the transition is inhomogeneously broadened, the gain is reduced by a factor of two when the signal intensity is given by

$$\frac{1}{\sqrt{1 + I/I_s}} = \frac{1}{2}$$

$$1 + \frac{I}{I_s} = 4$$

$$I = 3I_s = 4.88 \times 10^8 \text{ W/m}^2$$

19.7 Assuming uniform excitation, the gain in a length $L = 15 \text{ m}$ is $(1.5 \text{ dB/m})(15 \text{ m}) = 22.5 \text{ dB}$. Using Eq.(19-16), the unsaturated gain coefficient is found from

$$\gamma_0 L = \frac{22.5}{4.34} = 5.18$$

The gain of the amplifier is $G = (5 \times 10^5)/(2.5 \times 10^4) = 20$, and solving Eq.(19-27) for I_s then gives

$$I_s = \frac{I_1(G - 1)}{\gamma_0 L - \ln G} = \frac{(2.5 \times 10^4)(19)}{5.18 - \ln(20)} = 2.17 \times 10^5 \text{ W/cm}^2$$

20.5 (a) The threshold gain coefficient is

$$\gamma_{th} = \frac{1}{2L} \ln \left(\frac{1}{R_1 R_2} \right) = \frac{1}{2(0.2)} \ln \left(\frac{1}{[0.998][0.99]} \right) = 0.030 \text{ m}^{-1}$$

and the threshold population inversion is therefore

$$N_{2,th} = \frac{1}{c\sigma\tau_c} = \frac{\gamma_{th}}{\sigma} = \frac{3 \times 10^{-4} \text{ cm}^{-1}}{30 \times 10^{-14} \text{ cm}^2} = 1 \times 10^9 \text{ cm}^{-3}$$

The fraction of Ne atoms that need to be excited is therefore

$$\text{frac} = \frac{1 \times 10^9}{1.2 \times 10^{16}} = 8.3 \times 10^{-8}$$

(b) The number of atoms pumped to level 2 per unit time is $\mathcal{R}_{th}V$, where V is the volume of the gain medium. Using Eq.(20-18) we have

$$\mathcal{R}_{th}V = \frac{N_{2,th}V}{\tau_2} = \frac{(1 \times 10^9 \text{ cm}^{-3})(20 \text{ cm})\pi(5 \times 10^{-2} \text{ cm})^2}{1 \times 10^{-7} \text{ s}} = 1.57 \times 10^{15} \text{ s}^{-1}$$

(c) The minimum pump power required is

$$P_{in} = (1.57 \times 10^{15} \text{ s}^{-1})(20 \text{ eV})(1.6 \times 10^{-19} \text{ J/eV}) = 5 \times 10^{-3} \text{ W}$$

In practice, the electrical pumping power required is much larger, on the order of a few Watts, due to inefficient excitation of the upper laser level.

20.6 From Eq.(20-21), the light intensity inside the laser cavity is

$$I = \frac{2P_{out}}{AT} = \frac{2(1.5 \times 10^{-3})}{\pi(5 \times 10^{-4})^2(0.01)} = 3.82 \times 10^5 \text{ W/m}^2$$

The photon energy is

$$h\nu = \frac{hc}{\lambda} = \frac{(6.63 \times 10^{-34})(3 \times 10^8)}{632.8 \times 10^{-9}} = 3.14 \times 10^{-19} \text{ J}$$

The induced emission rate is therefore

$$W_{21}^{ind} = \frac{(3.82 \times 10^5)(3 \times 10^{-17})}{3.14 \times 10^{-19}} = 3.65 \times 10^7 \text{ s}^{-1}$$

The spontaneous emission rate is simply the inverse of the radiative lifetime,

$$W_{21}^{spont} = 1/(30 \times 10^{-9}) = 3.33 \times 10^7 \text{ s}^{-1}$$

The ratio is then $W_{21}^{ind}/W_{21}^{spont} = 3.65/3.33 = 1.1$

20.11 The condition that the pump be three times threshold is

$$\frac{P_{in}}{P_{th}} = \frac{\gamma_0 2L}{\delta + T} = 3$$

Eq.(20-32) then becomes

$$4 W = \frac{1}{2} AT I_s [3 - 1]$$

Solving for I_s then gives

$$I_s = \frac{2(4)}{AT[3 - 1]} = \frac{4}{\pi(5 \times 10^{-4})^2(0.005)} = 1.02 \times 10^9 \text{ W/m}^2$$