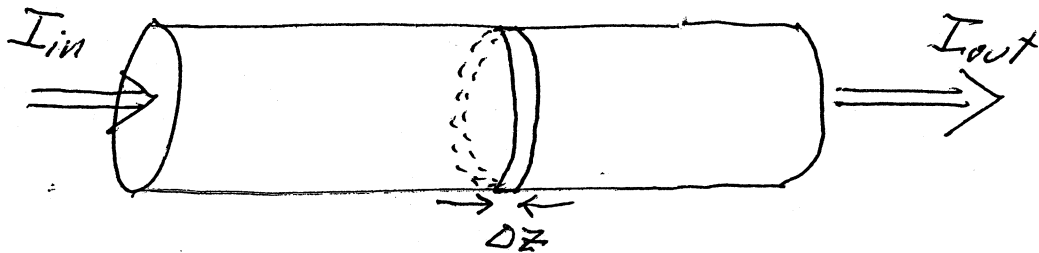


Optical Amplifiers



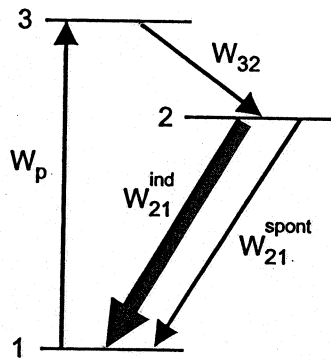
$$\frac{\Delta I}{I} = \gamma \Delta z$$

γ may not be constant (saturation)

$$\gamma = (N_2 - N_1) \sigma$$

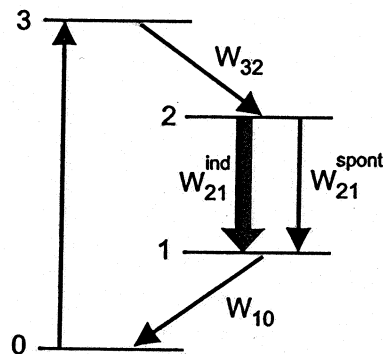
Use rate equations to determine N_1 & N_2

Two types of laser systems:



three-level system

example
ruby



four-level system

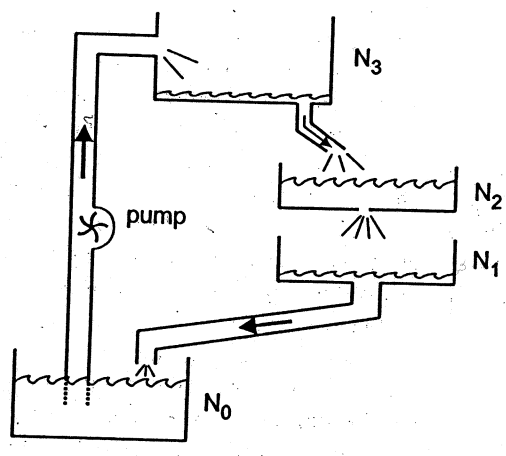
example
Nd:YAG

n-level system: lower laser level is ground state

For positive gain, need $N_2 > N_1$ (population inversion)

So n-level needs at least half of atoms in excited state \Rightarrow difficult to achieve

Flow of excitation energy similar to water flow:



larger holes \Rightarrow faster decay

$W_{p2} = \frac{1}{\tau_{p2}}$ etc.

Assume $\begin{cases} \tau_{32} \ll \tau_{21} \\ \tau_{10} \ll \tau_{21} \end{cases}$

$N_0 + N_2 \approx N$ total # atoms / Vol

so level 2 is "bottleneck"
 $N_3 \ll N_2$
 $N_1 \ll N_2$

Rate equation becomes

$$\frac{dN_2}{dt} = N_0 W_p - N_2 W_{21}^{ind} - N_2 \frac{1}{\tau_2}$$

Also assume for now $N_2 \ll N_0$, so $N_0 \approx N$ is constant

Total decay from level 2

$$W_2 = \frac{1}{\tau_2} = \frac{1}{\tau_{21}} + \frac{1}{\tau_{20}}$$

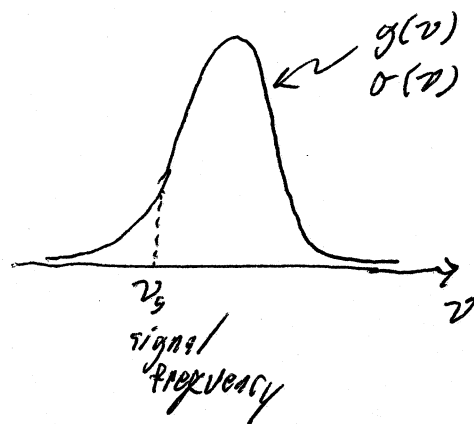
Assume for now little depletion of ground state:

$$N_2 \ll N_{\text{tot}}$$

Re-write rate eq. in terms of light intensity

$$\begin{aligned} W_{21}^{\text{ind}} &= B_{21} \rho_\nu g(\nu) \\ &= \left(\frac{A_{21}}{8\pi \nu^3} \frac{1}{c} \right) \left(\frac{I}{c} \right) g(\nu) \\ &= \left(\frac{A_{21} \lambda^2 g(\nu)}{8\pi} \right) \frac{I}{h\nu} \end{aligned}$$

$$W_{21}^{\text{ind}} = \frac{I \sigma(\nu)}{h\nu}$$



Define pumping rate

$$R \equiv W_p N_0 \quad \left[\frac{\text{atoms pumped}}{\text{Vol} \cdot \text{time}} \right]$$

Rate eq. becomes

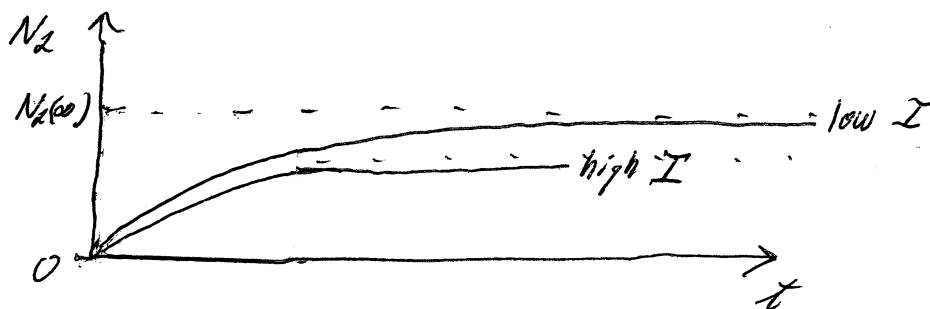
$$\frac{dN_2}{dt} = R - N_2 \left(\frac{I \sigma}{h\nu} + \frac{1}{\tau_2} \right)$$

$$\text{or} \quad \frac{dN_2}{dt} = R - \frac{N_2}{\tau_2'}$$

$$\frac{1}{\tau_2'} \equiv \frac{1}{\tau_2} + \frac{I \sigma}{h\nu}$$

This diff eq similar to that for charging cap:

$$N_2(t) = N_2(\infty) [1 - e^{-t/\tau_2'}]$$



Solve for $N_2(\infty)$ by setting $\frac{dN_2}{dt} = 0$

$$0 = R - \frac{N_2}{\tau_2'}$$

$$N_2(\infty) = R \tau_2'$$

$$= \frac{R}{\frac{1}{\tau_2} + \frac{I\sigma}{h\nu}} = \frac{R \tau_2}{1 + \frac{I\sigma}{h\nu} \tau_2}$$

Note: as I increases, N_2 rises more quickly (τ_2' decreases), but to a smaller final value.

Steady-state value $N_2(\infty)$ important, since it limits gain:

$$\frac{1}{I} \frac{dI}{dz} \equiv \delta(\nu) = A_{21} \frac{\lambda^2}{8\pi} g(\nu) N_2 = \sigma(\nu) N_2$$

$$\delta(\nu) = \frac{R \sigma(\nu) \tau_2}{1 + \frac{I\sigma \tau_2}{h\nu}}$$

Define "saturation intensity" where gain drops by factor of 2:

$$\frac{I_s \sigma \tau_2}{h\nu} = 1$$

$$I_s = \frac{h\nu}{\sigma \tau_2}$$

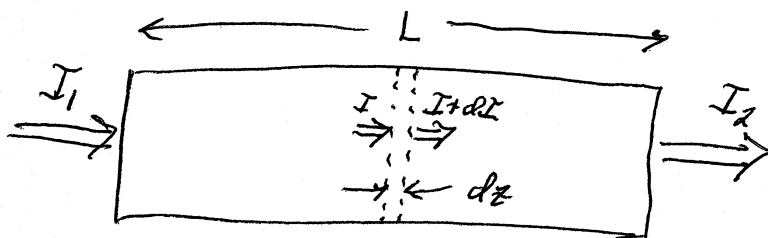
Then can write

$$\delta = \frac{R \sigma \tau_2}{1 + I/I_s} = \frac{\delta_0}{1 + I/I_s}$$

where $\delta_0 \equiv R \sigma \tau_2$

Note: long τ_2 gives higher small signal gain but gain saturation occurs at lower I

Total Gain of Optical Amplifier



$$\frac{1}{I} \frac{dI}{dz} = \frac{\delta_0}{1 + \frac{I}{I_s}}$$

Two limits;

(1) Small signal $I \ll I_s$

$$\left\{ \frac{dI}{I} \right\} \approx \int \delta_0 dz$$

$$\ln I \Big|_{I_1}^{I_2} = \delta_0 z \Big|_0^L$$