# WORCESTER POLYTECHNIC INSTITUTE MECHANICAL ENGINEERING DEPARTMENT

#### Engineering Experimentation ME-3901, D'2012

Lecture 06 26 March 2012





### General information

Office hours

<u>Instructors</u>: Cosme Furlong Office: HL-151 <u>Everyday</u>: 9:00 to 9:50 am Christopher Scarpino Office: HL-153 During laboratory sessions

<u>Teaching Assistants</u>: During laboratory sessions





### Error versus uncertainty

- Errors are based on knowledge of actual values (or standard values). <u>Statistics</u> are used
- Uncertainties are evaluated <u>analytically</u>
  - there are a number of procedures for determination of the overall uncertainty
  - the most popular and most widely used relationship for determination of uncertainty is known of the RSS-type
  - the relationship defining the RSS-type overall uncertainty is based on a partial differential representation





#### Precision uncertainty

Governing equation to use is:

$$R = \frac{V}{I}$$

Phenomenological equation is, therefore, R = R(V, I)

**ASME method:** Square-root of the sum-of-the squares (RSS) approach indicates that the uncertainty,  $\delta R$ , in R, can be determined as

$$\delta R = \left[ \left( \frac{\partial R}{\partial V} \delta V \right)^2 + \left( \frac{\partial R}{\partial I} \delta I \right)^2 \right]^{1/2}$$

Uncertainty in measured voltage is:  $\delta V$ Uncertainty in provided voltage is:  $\delta I$ 



#### Precision uncertainty

Individual partial derivates are: 
$$\frac{\delta R}{\partial V} = \frac{1}{I}; \quad \frac{\delta R}{\partial I} = -\frac{V}{I^2}$$

Substitute:

$$\delta R = \left[ \left( \frac{1}{I} \,\delta V \right)^2 + \left( -\frac{V}{I^2} \,\delta I \right)^2 \right]^{1/2}$$

Normalized uncertainty is:

$$\frac{\delta R}{R} = \left[ \left( \frac{1}{V} \delta V \right)^2 + \left( -\frac{1}{I} \delta I \right)^2 \right]^{1/2}$$

**Problem:** estimate uncertainty and normalized uncertainty in measurements of electrical resistance (as done in Lab #1). Assume: (a) measuring range [-10,10] V; (b) 12-bit digitization; (c) measured voltage of 0.11 V; (d) I = 1 mA; half the least significant digit for  $\delta I$ ; (e) determine  $R \pm \delta R$ <u>Discuss your results</u>.



#### Precision uncertainty

Consider the problem of measuring the electrical resistance of a component (as done in Lab #1); governing equation used to determine  $R_2$  is:





### RSS-type uncertainty: example

Consider a solid block with dimensions of L, W, and H, as shown in the figure. The block is placed in the environment at temperature of 20°C where the convective heat transfer coefficient is 15 $\pm$ 3 W/m<sup>2</sup>-°C.  $\blacklozenge$  Z The block is at the temperature of  $300 \pm 5^{\circ}$ C. Determine the magnitude of the heat transfer by convection,  $Q_c$ , from the top surface of the block and the corresponding overall uncertainty in this magnitude. Also, list in descending order percentage contributions to the overall uncertainty in  $Q_c$  due to the individual uncertainties.





### RSS-type uncertainty

Consider *explicit equation* for convective heat transfer:

$$Q_c = hA_c \left(T_s - T_e\right)$$

This equation can be represented, in the most general way, by the *fundamental equation*, also known as *phenomenological equation*, as follows:

$$Q_c = Q_c(h, A_c, T_s, T_e)$$

The RSS-type uncertainty, based on the above equation, can be expressed as

$$\delta Q_c = \left[ \left( \frac{\partial Q_c}{\partial h} \, \delta h \right)^2 + \left( \frac{\partial Q_c}{\partial A_c} \, \delta A_c \right)^2 + \left( \frac{\partial Q_c}{\partial T_s} \, \delta T_s \right)^2 + \left( \frac{\partial Q_c}{\partial T_e} \, \delta T_e \right)^2 \right]^{\frac{1}{2}}$$

where the symbol  $\delta$  denotes the uncertainty



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$$A_c = LW = (1.4 \ m)(0.25 \ m) = 0.35 \ m^2$$
$$Q_c = hA_c \left(T_s - T_e\right) = \left(15 \ \frac{W}{m^2 \circ C}\right) (0.35 \ m^2) (300 - 20)^\circ C = 1,470 \ W$$

The fundamental equation is

$$Q_c = Q_c(h, A_c, T_s, T_e)$$

The RSS-type overall uncertainty can be determined from

$$\delta Q_{c} = \left[ \left( \frac{\partial Q_{c}}{\partial h} \, \delta h \right)^{2} + \left( \frac{\partial Q_{c}}{\partial A_{c}} \, \delta A_{c} \right)^{2} + \left( \frac{\partial Q_{c}}{\partial T_{s}} \, \delta T_{s} \right)^{2} + \left( \frac{\partial Q_{c}}{\partial T_{e}} \, \delta T_{e} \right)^{2} \right]^{\frac{1}{2}}$$

or

$$\delta Q_c = \left(\partial Q_c \,\delta h^2 + \partial Q_c \,\delta A_c^2 + \partial Q_c \,\delta T_s^2 + \partial Q_c \,\delta T_s^2\right)^{\frac{1}{2}}$$



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$$\partial Q_c \,\delta h^2 = \left(\frac{\partial Q_c}{\partial h} \,\delta h\right)^2 = \left[A_c \left(T_s - T_e\right) \delta h\right]^2 = \qquad \delta h = \pm 3 \frac{W}{m^2 \circ C}$$
$$= \left\{ \left(0.35 \ m^2\right) \left[ (300 - 20)^\circ C \right] \left(3 \frac{W}{m^2 \circ C}\right) \right\}^2 = 8.64360 \times 10^4 \ W^2$$

$$\partial Q_c \delta A_c^2 = \left(\frac{\partial Q_c}{\partial A_c} \delta A_c\right)^2 = [h(T_s - T_e)\delta A_c]^2$$

$$A_c = LW \longrightarrow A_c = A_c(L, W)$$

$$\delta A_{c} = \left[ \left( \frac{\partial A_{c}}{\partial L} \, \delta L \right)^{2} + \left( \frac{\partial A_{c}}{\partial W} \, \delta W \right)^{2} \right]^{\frac{1}{2}}$$



$$\delta A_{c} = \left[ \left( \frac{\partial A_{c}}{\partial L} \, \delta L \right)^{2} + \left( \frac{\partial A_{c}}{\partial W} \, \delta W \right)^{2} \right]^{\frac{1}{2}}$$

$$\delta A_c = \left[ (W \delta L)^2 + (L \delta W)^2 \right]^{\frac{1}{2}} = \left\{ \left[ (0.25 \ m)(0.03 \ m) \right]^2 + \left[ (1.4 \ m)(0.01 \ m) \right]^2 \right\}^{\frac{1}{2}} = \left\{ (5.62500 \times 10^{-5} \ m^2 + 1.96000 \times 10^{-4} \ m^2)^{\frac{1}{2}} = 1.58824 \times 10^{-2} \ m^2 \right\}^{\frac{1}{2}}$$

$$\partial Q_c \delta A_c^2 = \left[h(T_s - T_e)\delta A_c\right]^2 = \left\{ \left(15 \frac{W}{m^2 \circ C}\right) \left[(300 - 20)^\circ C\right] \left(1.58824 \times 10^{-2} \ m^2\right) \right\}^2 = 4.44970 \times 10^3 \ W^2$$





$$\partial Q_c \delta T_s^2 = \left(\frac{\partial Q_c}{\partial T_s} \delta T_s\right)^2 = \left(hA_c \delta T_s\right)^2 = \delta T_s = \pm 5 \,^{\circ}C$$
$$= \left[\left(15 \,\frac{W}{m^2 \,^{\circ}C}\right) \left(0.35 \,m^2\right) \left(5 \,^{\circ}C\right)\right]^2 = 6.89063 \times 10^2 \,W^2$$

$$\partial Q_c \, \delta T_e^2 = \left(\frac{\partial Q_c}{\partial T_e} \, \delta T_e\right)^2 = \left(-hA_c \, \delta T_e\right)^2 = \frac{\delta T_e = \pm 0.5 \,^\circ C}{\left[\frac{1}{2} \text{LSD}\right]^2} = \left[-\left(15 \, \frac{W}{m^2 \,^\circ C}\right) \left(0.35 \, m^2\right) \left(0.5 \,^\circ C\right)\right]^2 = 6.89063 \times 10^0 \, W^2$$





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$$\delta Q_c = \left(\partial Q_c \delta h^2 + \partial Q_c \delta A_c^2 + \partial Q_c \delta T_s^2 + \partial Q_c \delta T_s^2\right)^{\frac{1}{2}} = \\ = \left[ \left( 8.64360 \times 10^4 + 4.44970 \times 10^3 + 6.89063 \times 10^2 + 6.89063 \times 10^0 \right) W^2 \right]^{\frac{1}{2}} = \\ = 3.02625 \times 10^2 W = 302.6 W \qquad \longrightarrow \qquad \text{This is the overall uncertainty}$$

The percentage overall uncertainty is

$$\% \delta Q_c = \frac{\delta Q_c}{Q_c} \times 100\% = \frac{302.6 W}{1,470 W} \times 100\% = \frac{20.6\%}{100\%}$$

The percentage contributions of the individual uncertainties to the overall uncertainty can be computed as

$$\% \partial Q_c \delta h = \frac{\partial Q_c \delta h^2}{\delta Q_c^2} \times 100\% = \frac{8.64360 \times 10^4 W^2}{\left(3.02625 \times 10^2 W\right)^2} \times 100\% = 94.3811\%$$



 $CHECK = \% \partial Q_c \delta h + \% \partial Q_c \delta A_c + \% \partial Q_c \delta T_s + \% \partial Q_c \delta T_e =$ = 94.3811\% + 4.8587\% + 0.7524\% + 0.0075\% = 99.9997\% \approx 100.0\%



