

ME-3901. Engineering Experimentation

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Initial parameters:

$$\begin{aligned} t &:= 0.003 & (\text{in}) & & \delta t &:= 5 \cdot 10^{-4} \\ r &:= 1.28 & (\text{in}) & & \delta r &:= 5 \cdot 10^{-3} \\ E &:= 10.0 \cdot 10^6 & (\text{lbf/in}^2) & & \delta E &:= 0.1 \cdot E & \delta E &= 1 \times 10^6 \\ \nu &:= 0.3 & & & \delta \nu &:= 0.05 \\ & & & & \delta \epsilon_s &:= 25 \cdot 10^{-6} & (\text{microstrain}) \end{aligned}$$

Define range for strain:

$$\epsilon_s := 10 \cdot 10^{-6}, 20 \cdot 10^{-6} \dots 2000 \cdot 10^{-6}$$

$$P(\epsilon_s) := E \cdot t \cdot \frac{\epsilon_s}{\left(1 - \frac{\nu}{2}\right) \cdot r}$$

Define partial derivatives functions:

$$fE(\epsilon_s) := t \cdot \frac{\epsilon_s}{r \cdot \left(1 - \frac{\nu}{2}\right)}$$

$$fthi(\epsilon_s) := E \cdot \frac{\epsilon_s}{r \cdot \left(1 - \frac{\nu}{2}\right)}$$

$$fes(\epsilon_s) := E \cdot \frac{t}{r \cdot \left(1 - \frac{\nu}{2}\right)}$$

$$fra(\epsilon_s) := -E \cdot t \cdot \frac{\epsilon_s}{r^2 \cdot \left(1 - \frac{\nu}{2}\right)}$$

$$fv(\epsilon_s) := \frac{1}{2} \cdot E \cdot t \cdot \frac{\epsilon_s}{r \cdot \left(1 - \frac{\nu}{2}\right)^2}$$

Uncertainty in pressure as a function of strain:

$$\delta P1(\epsilon_s) := (fE(\epsilon_s) \cdot \delta E)^2 + (fthi(\epsilon_s) \cdot \delta t)^2 + (fes(\epsilon_s) \cdot \delta \epsilon_s)^2 + (fra(\epsilon_s) \cdot \delta r)^2 + (fv(\epsilon_s) \cdot \delta \nu)^2$$

$$\delta P(\epsilon_s) := \delta P1(\epsilon_s)^{0.5}$$

Uncertainty as a function of strain

$$\delta P(1370 \cdot 10^{-6}) = 7.459$$

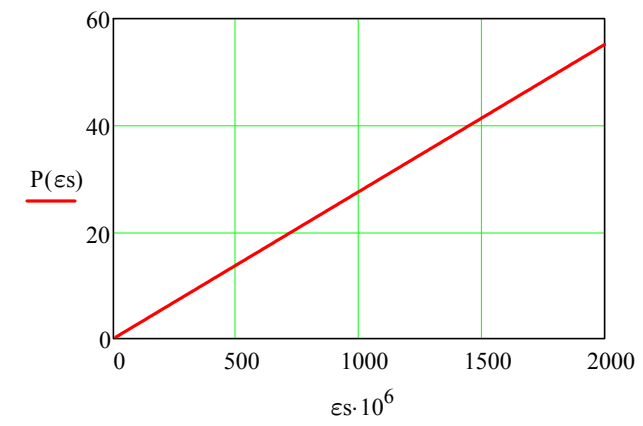
(Example: strain at 1370 microstrains)

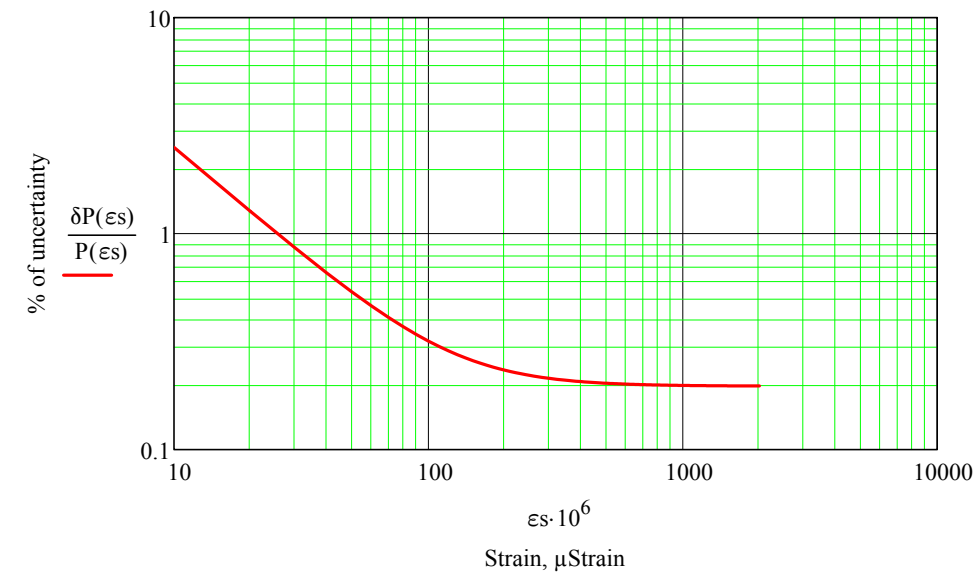
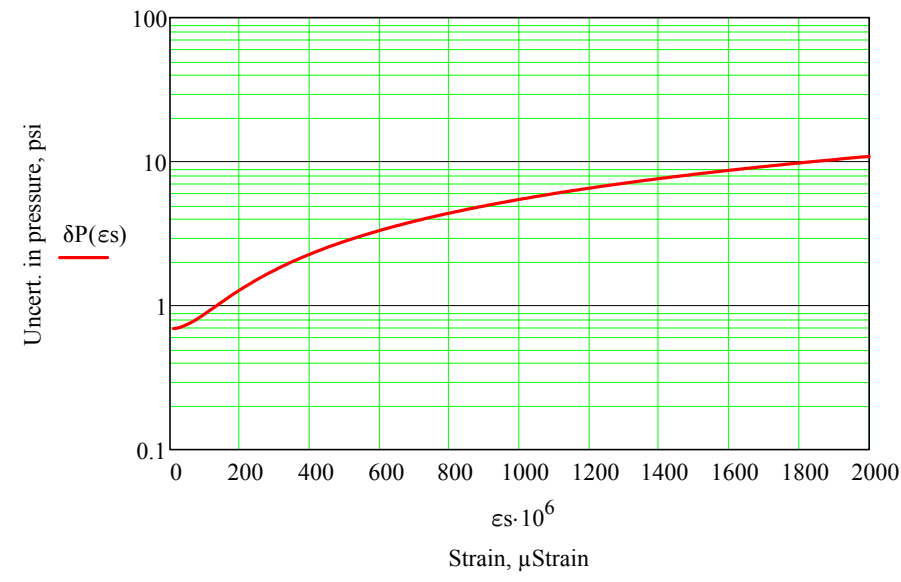
$$P(1370 \cdot 10^{-6}) = 37.776 \quad fra(1370 \cdot 10^{-6}) \cdot \delta r = -0.148 \quad fv(1370 \cdot 10^{-6}) \cdot \delta \nu = 1.111$$

$$fE(1370 \cdot 10^{-6}) \cdot \delta E = 3.778 \quad fthi(1370 \cdot 10^{-6}) \cdot \delta t = 6.296 \quad fes(1370 \cdot 10^{-6}) \cdot \delta \epsilon_s = 0.689$$

(Example: pressure at 1370 microstrains)

$$P(1370 \cdot 10^{-6}) = 37.776 \quad (\text{psi})$$





Percentage contributions:

$$PIE(\epsilon_s) := \left(\frac{fE(\epsilon_s) \cdot \delta E}{\delta P(\epsilon_s)} \right)^2 \quad Pthi(\epsilon_s) := \left(\frac{fthi(\epsilon_s) \cdot \delta t}{\delta P(\epsilon_s)} \right)^2 \quad Ples(\epsilon_s) := \left(\frac{fes(\epsilon_s) \cdot \delta \epsilon_s}{\delta P(\epsilon_s)} \right)^2$$

$$PIra(\epsilon_s) := \left(\frac{fira(\epsilon_s) \cdot \delta r}{\delta P(\epsilon_s)} \right)^2 \quad Plv(\epsilon_s) := \left(\frac{fv(\epsilon_s) \cdot \delta v}{\delta P(\epsilon_s)} \right)^2$$

$$TU(\epsilon_s) := PIE(\epsilon_s) + Pthi(\epsilon_s) + Ples(\epsilon_s) + PIra(\epsilon_s) + Plv(\epsilon_s)$$

$$PcPIE(\epsilon_s) := 100 \cdot \frac{PIE(\epsilon_s)}{TU(\epsilon_s)} \quad PcPthi(\epsilon_s) := 100 \cdot \frac{Pthi(\epsilon_s)}{TU(\epsilon_s)} \quad PcPles(\epsilon_s) := 100 \cdot \frac{Ples(\epsilon_s)}{TU(\epsilon_s)}$$

$$PcPIra(\epsilon_s) := 100 \cdot \frac{PIra(\epsilon_s)}{TU(\epsilon_s)} \quad PcPlv(\epsilon_s) := 100 \cdot \frac{Plv(\epsilon_s)}{TU(\epsilon_s)}$$

$$Check(\epsilon_s) := PcPIE(\epsilon_s) + PcPthi(\epsilon_s) + PcPles(\epsilon_s) + PcPIra(\epsilon_s) + PcPlv(\epsilon_s)$$

(to make sure it adds 100 %)

Order of importance for the numerical data used:

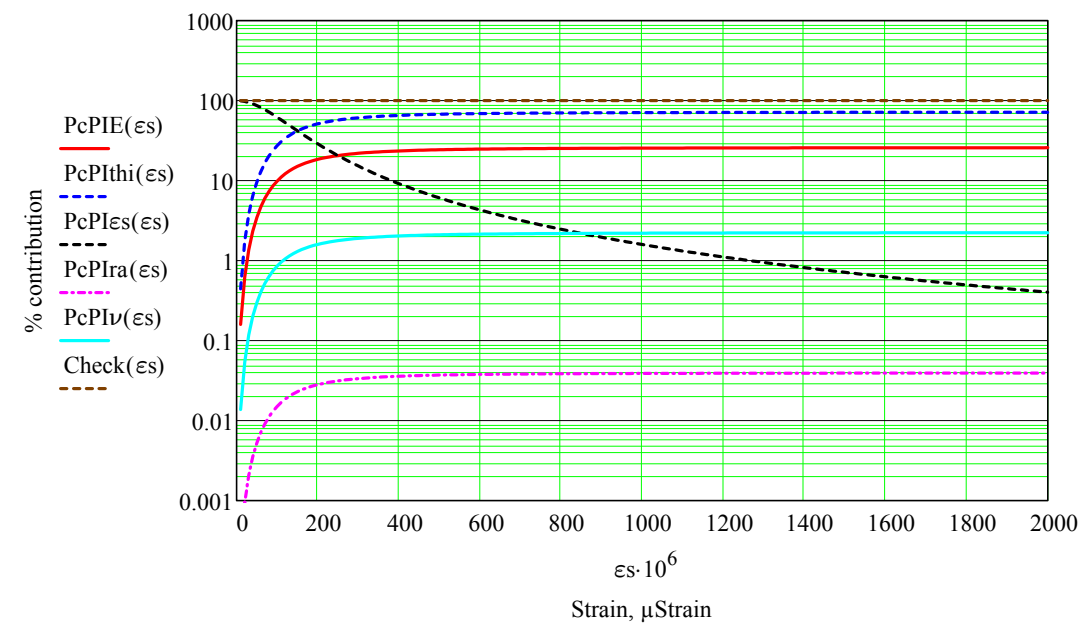
$$PcPthi(600 \cdot 10^{-6}) = 68.767$$

$$PcPIE(600 \cdot 10^{-6}) = 24.756$$

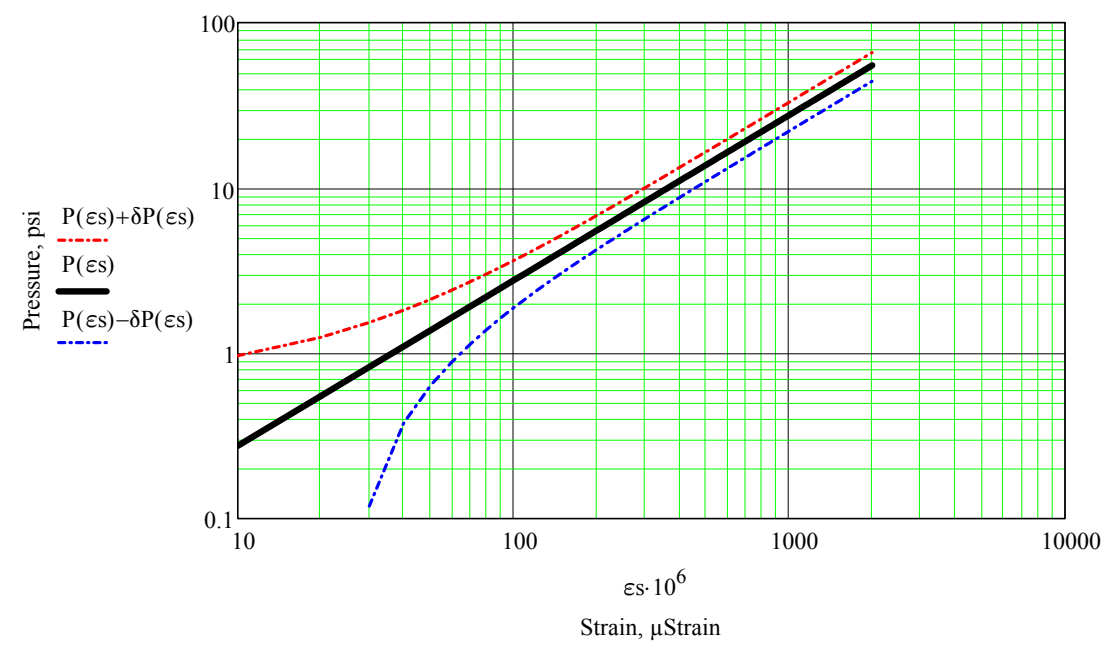
$$PcPles(600 \cdot 10^{-6}) = 4.298 \quad \text{(Example: evaluated at 600 microstrains)}$$

$$PcPlv(600 \cdot 10^{-6}) = 2.142$$

$$PcPIra(600 \cdot 10^{-6}) = 0.038$$



(Note that uncertainty range is greater at low values of strain.
This can be clearly seen when using a log-log scale)



Order of importance for the numerical data used:

$$PcPIEs(100 \cdot 10^{-6}) = 61.784$$

$$PcPlthi(100 \cdot 10^{-6}) = 27.46$$

$$PcPIE(100 \cdot 10^{-6}) = 9.886 \quad \text{(Example: evaluated at 100 microstrains)}$$

$$PcPIv(100 \cdot 10^{-6}) = 0.855$$

$$PcPIra(100 \cdot 10^{-6}) = 0.015$$

At low levels of strain:

$$P(200 \cdot 10^{-6}) = 5.515$$

$$\delta P(200 \cdot 10^{-6}) = 1.285$$

$$\frac{\delta P(200 \cdot 10^{-6})}{P(200 \cdot 10^{-6})} = 0.233$$

At higher levels of strain:

$$\delta P(1600 \cdot 10^{-6}) = 8.702$$

$$P(1600 \cdot 10^{-6}) = 44.118$$

$$\frac{\delta P(1500 \cdot 10^{-6})}{P(1500 \cdot 10^{-6})} = 0.197$$