

WORCESTER POLYTECHNIC INSTITUTE MECHANICAL ENGINEERING DEPARTMENT

DESIGN OF MACHINE ELEMENTS ME-3320, B'2022

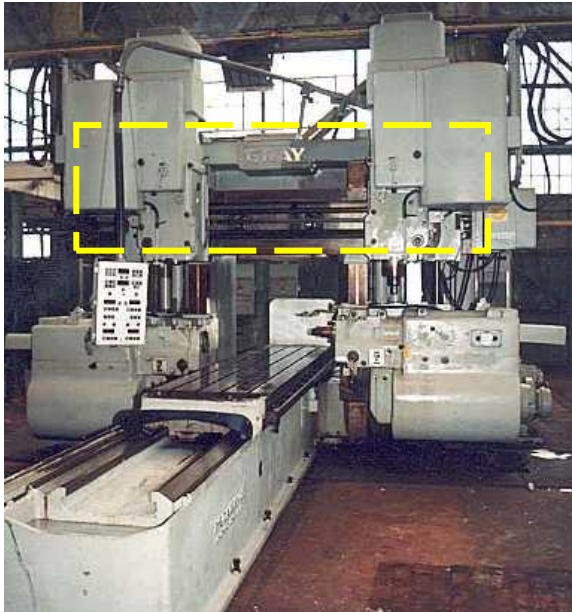
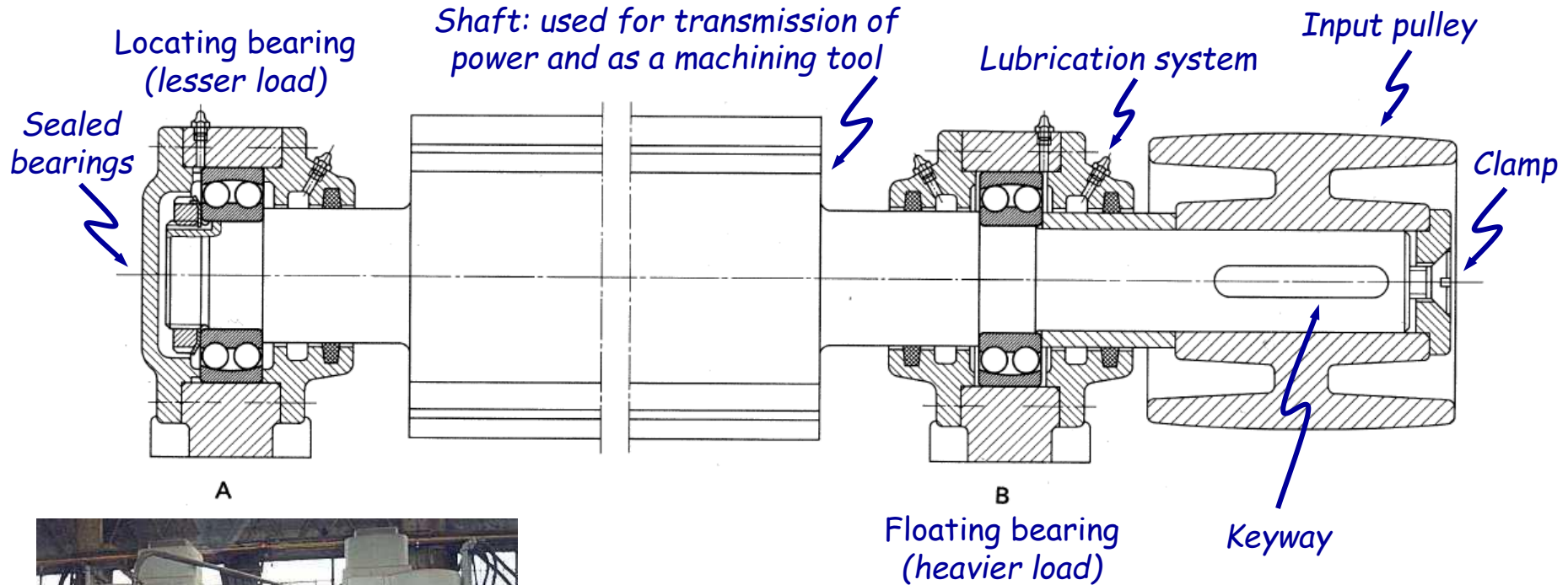
Lecture 20

December 2022

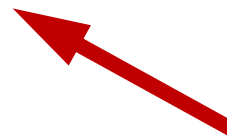


Shaft design

Example of rotating machinery: self-aligning ball bearings



- **Cutter shaft of a planer:** shaft diameter (at bearings locations) is 40 mm. Input power is 12 HP at maximum speed of 4,500 rpm



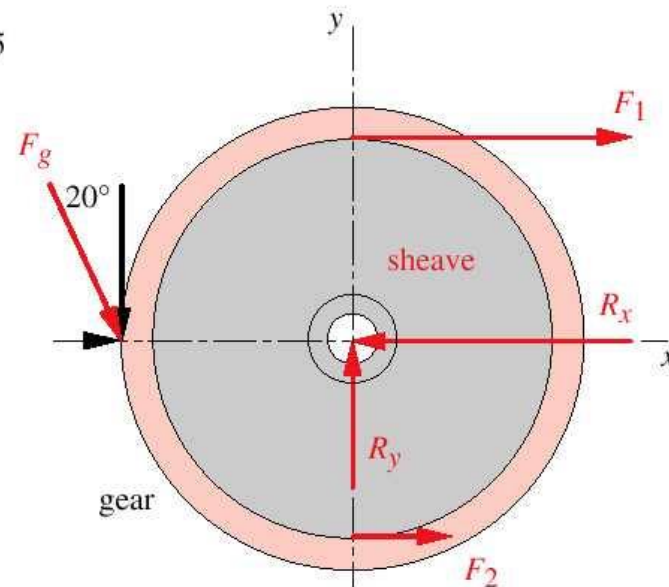
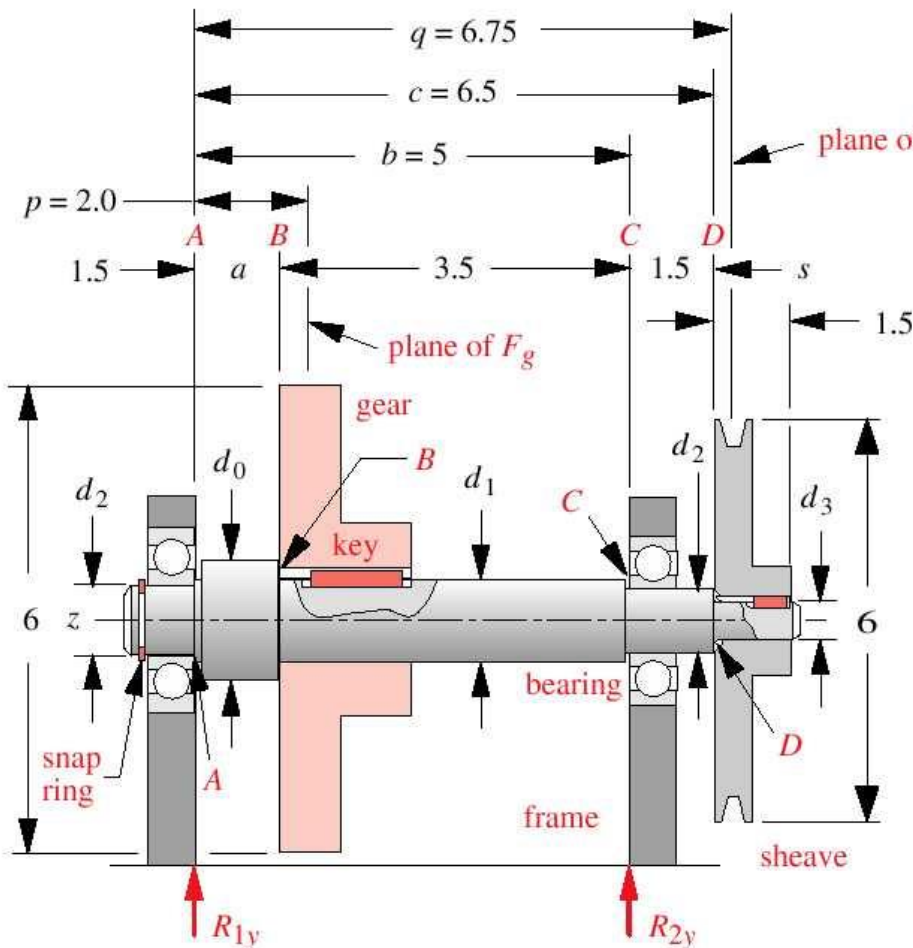
Shaft design

Fully-reversed bending and constant torsion

Review and Master: Example 10-1

Design shaft to support attachments

- Safety factor: 2.5
- Infinite life
- Material: SAE 1020 (good notch sensitivity)
- Operating conditions: room temperature
- Power: 2 HP at 1,750 rpm
- SCF of 3.5 for radii in bending, 2 in torsion, and 4 at the keyway
- Assume notch radius of 0.01 in



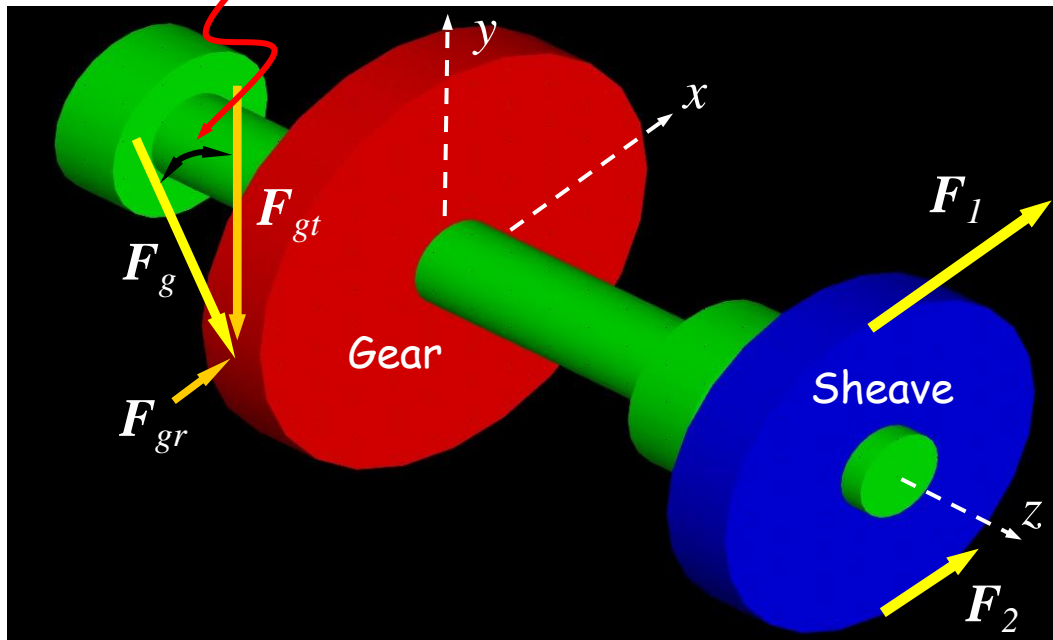
not to scale

Shaft design

Fully-reversed bending and constant torsion

□ Review and Master: Example 10-1

Pressure angle



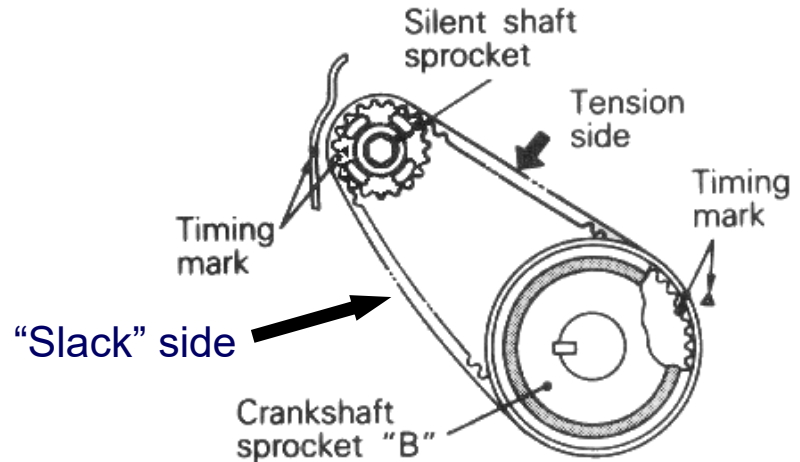
- Safety factor: 2.5
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- Material: SAE 1020 (good notch sensitivity)
- Operating conditions: room temperature
- Power: 2 HP at 1,750 rpm
- SCF of 3.5 for radii in bending, 2 in torsion, and 4 at the keyway
- Assume notch radius of 0.01 in

Tension & slack side components of the net force

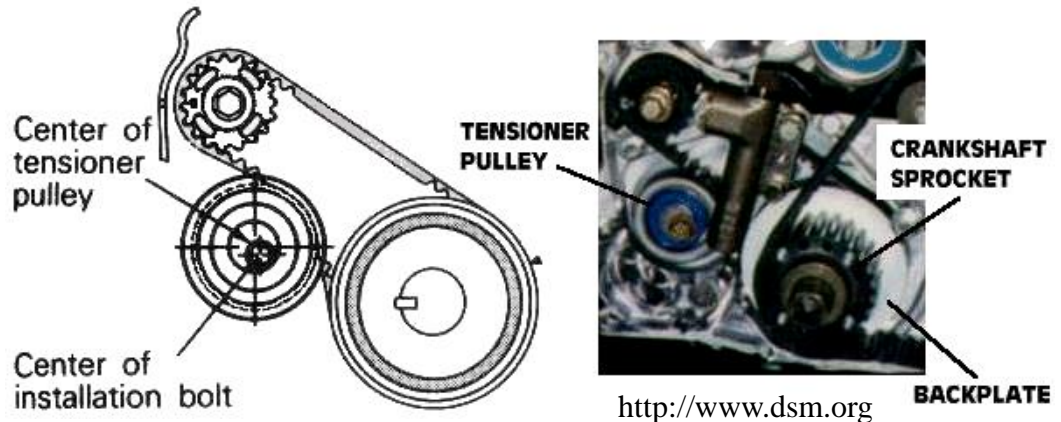
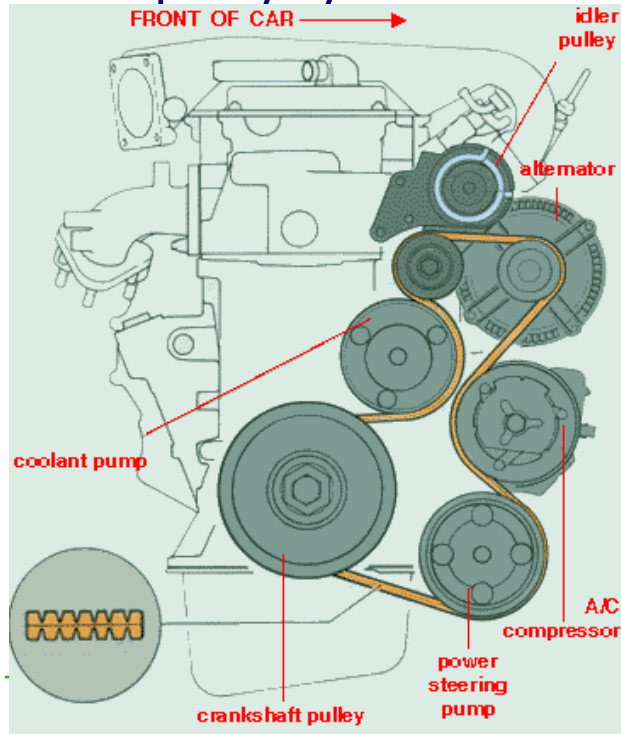


Shaft design: components. Examples 10-1 and 10-2

V-belt pulley



V-belt pulley system in a car




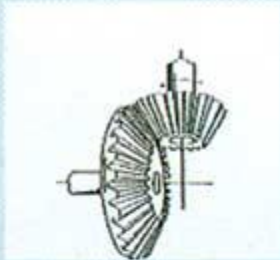


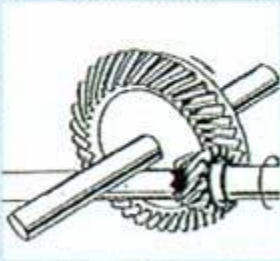
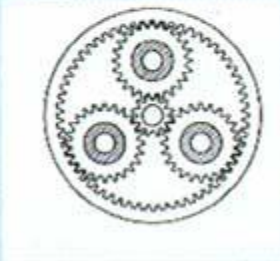

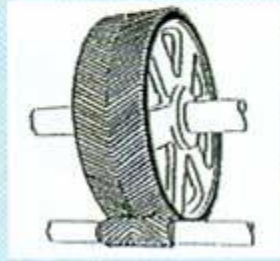
Shaft design: components. Examples 10-1 and 10-2

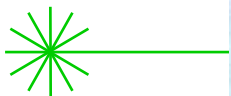
Spur



Helical



 <p>Spur Gears Transmissions</p>	 <p>Straight Bevel Gears Industrial Equipment Some Differentials</p>	 <p>Spiral Bevel Gears Industrial Equipment Some Differentials</p>	 <p>Worm Gear Set Gear Reduction Boxes</p>
 <p>Hypoid Gears Differentials</p>	 <p>Planetary Gear Set Transmissions</p>	 <p>Helical Gears Transmissions</p>	 <p>Herringbone Gears Transmissions</p>



Shaft design: components. Examples 10-1 and 10-2

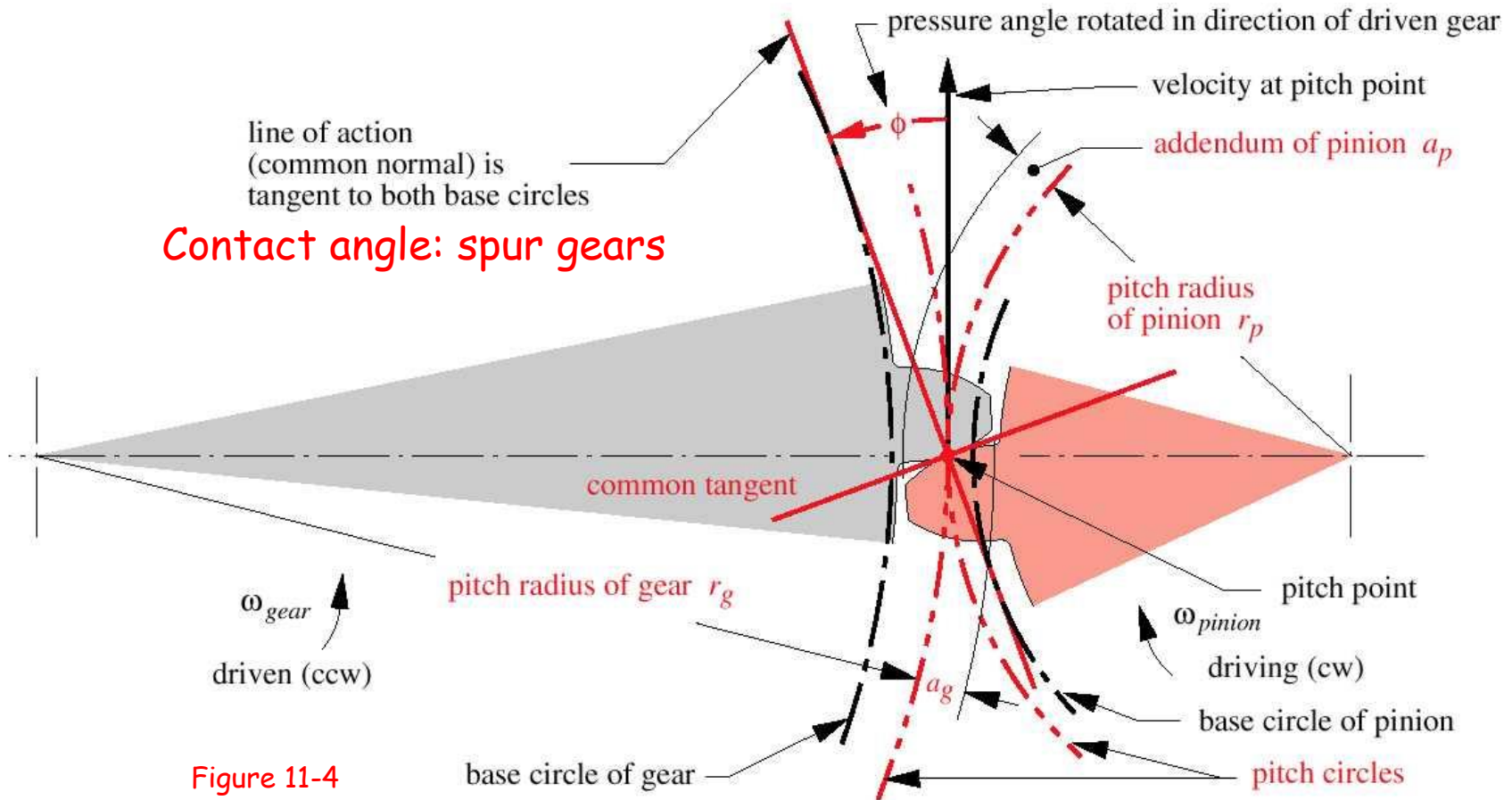


Figure 11-4



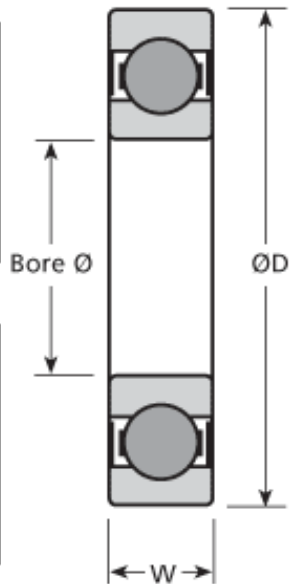
Shaft design: components. Examples 10-1 and 10-2

Radial ball bearings

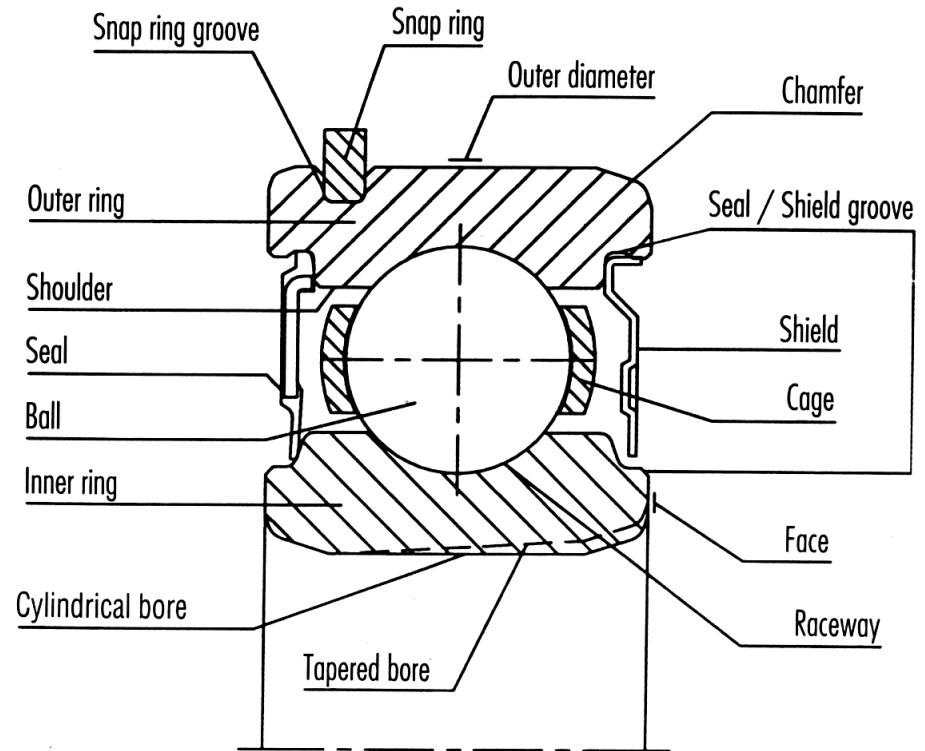
S Type Open



S-ZZ Type Shielded

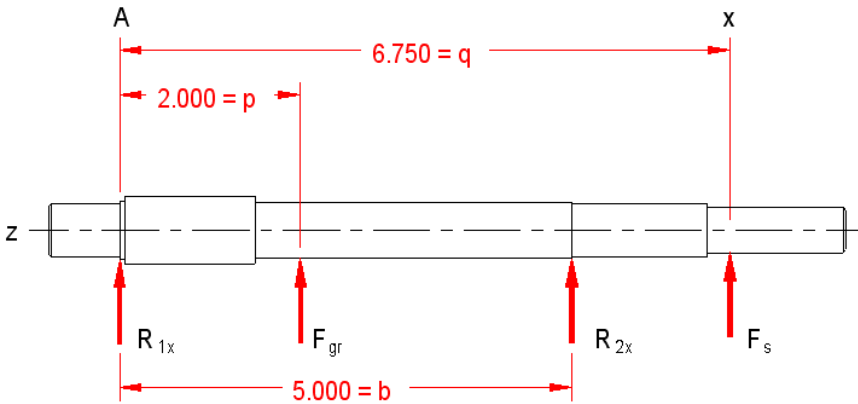


Cross-section of a radial ball-bearing

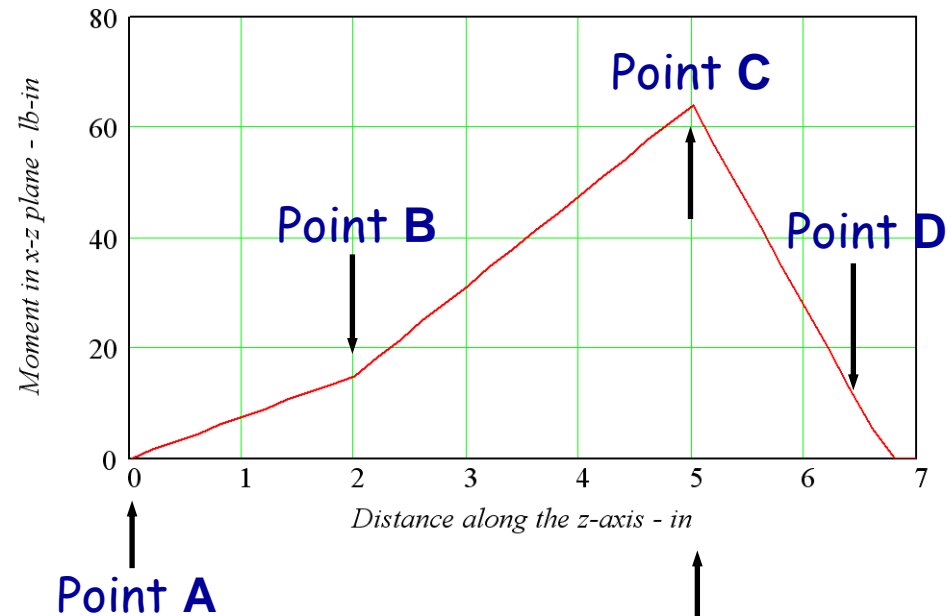


Shaft design: components. Examples 10-1 and 10-2

□ Load diagram in the X-Z plane

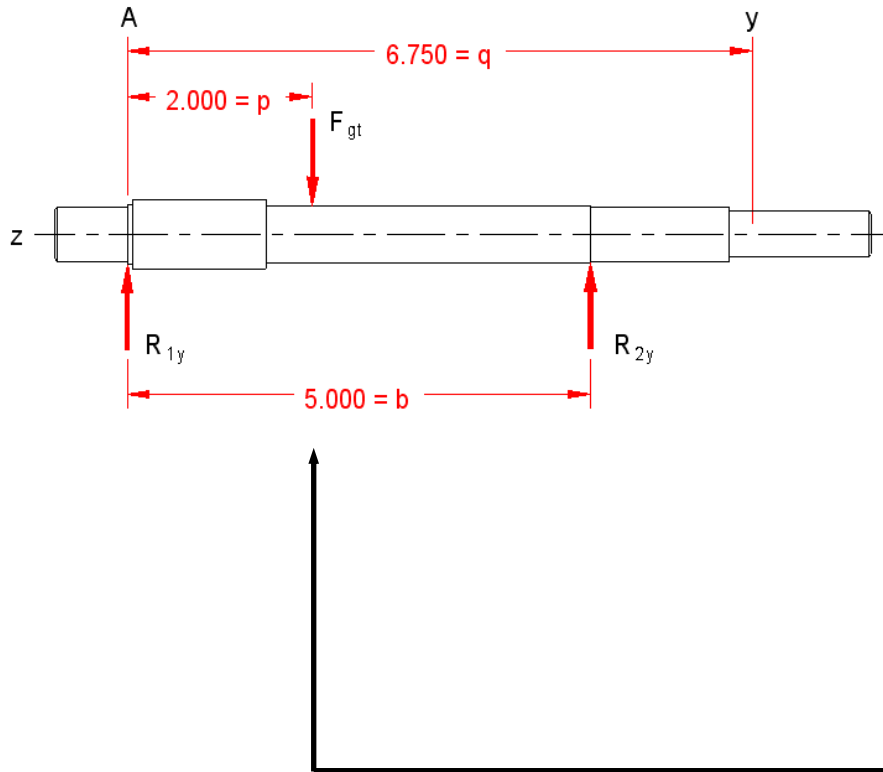


Moments diagram, X-Z plane

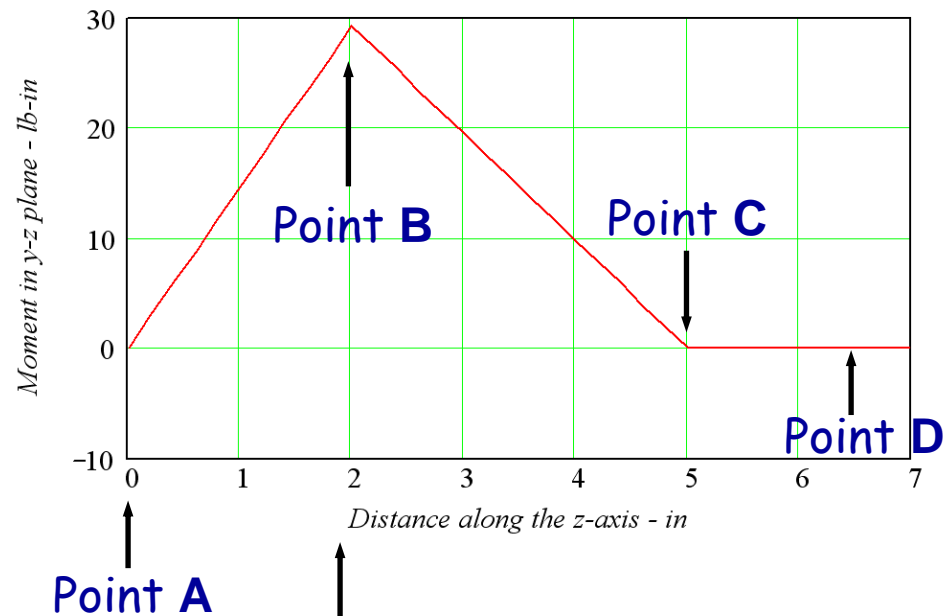


Shaft design: components. Examples 10-1 and 10-2

□ Load diagram in the Y-Z plane



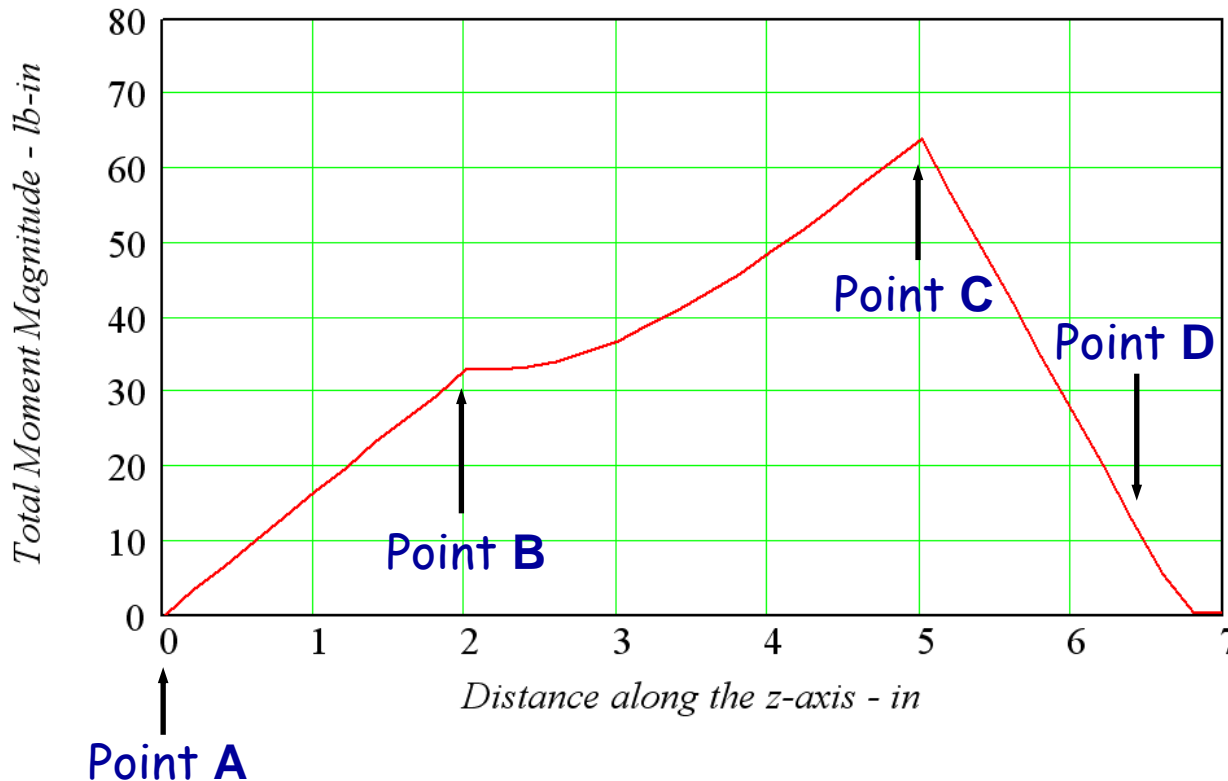
Moments diagram, Y-Z plane

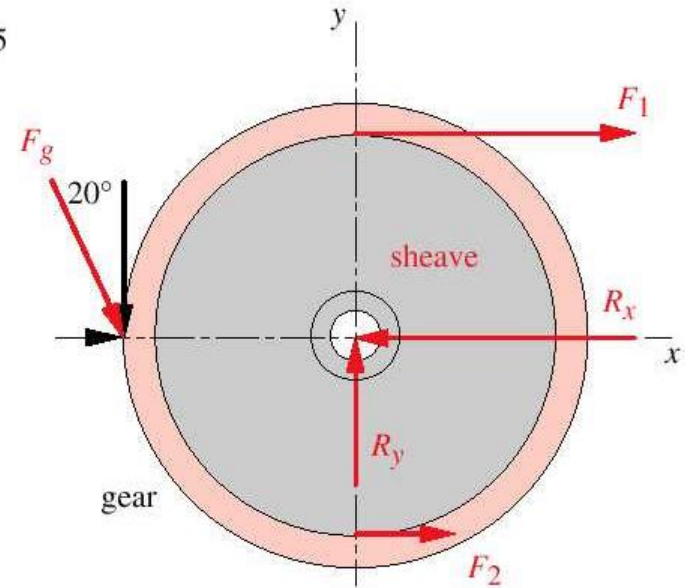
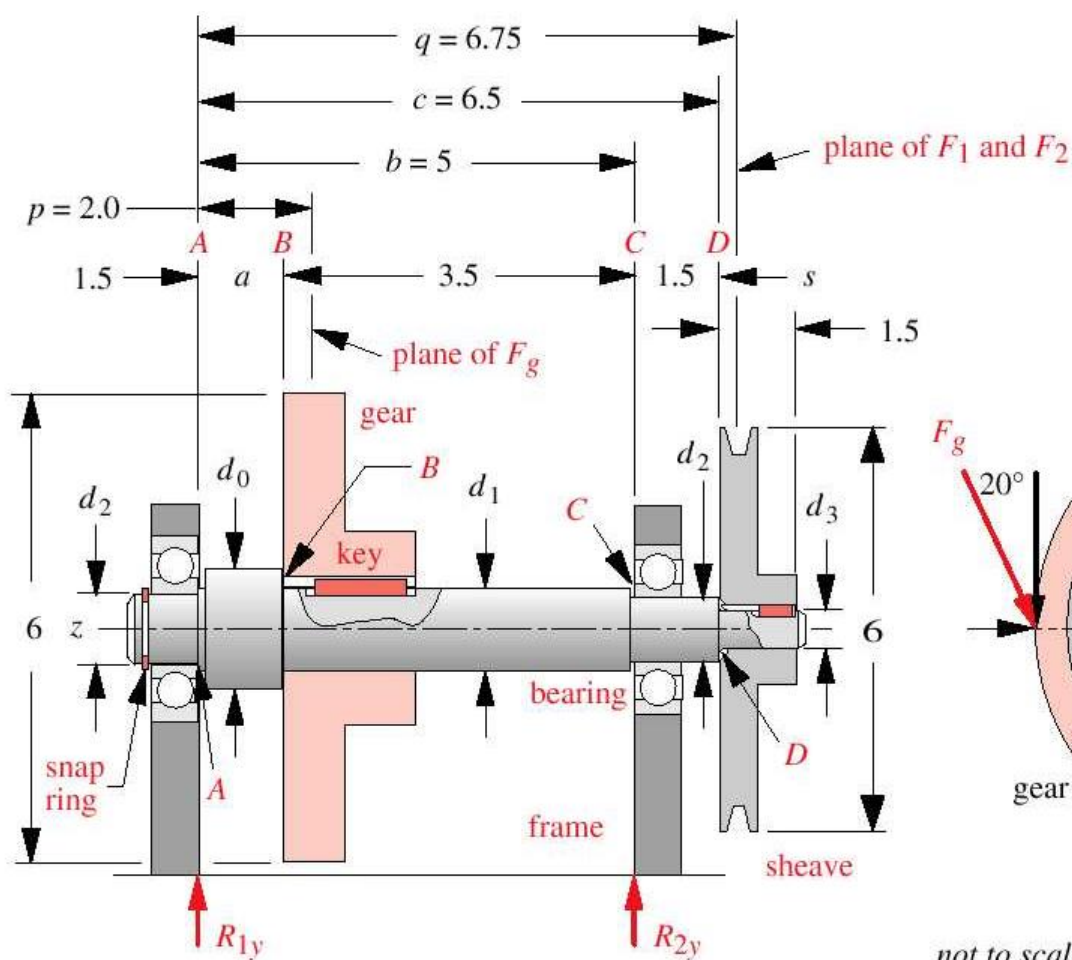


Shaft design: components. Examples 10-1 and 10-2

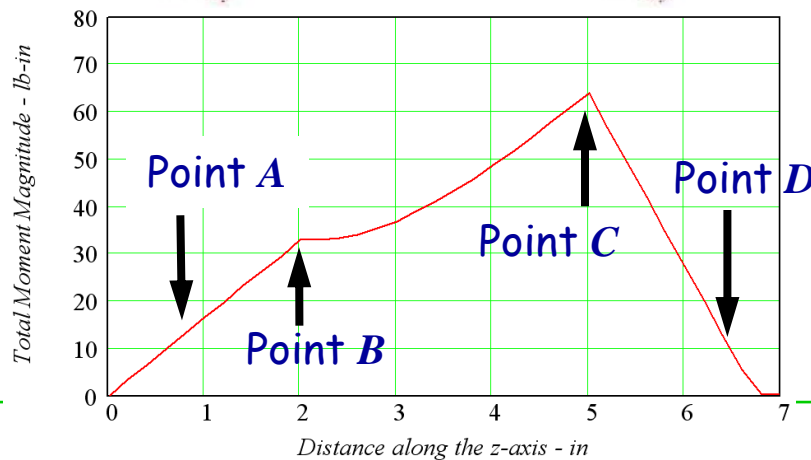
- **Total moment diagram:** note that the Amplitude & Mean components of the moments (and torque) require evaluation

$$M_T(z) = \left[M_{X-Z}^2 + M_{Y-Z}^2 \right]^{1/2}$$





not to scale



Total moment:

$$M_T(z) = \left[M_{X-Z}^2 + M_{Y-Z}^2 \right]^{1/2}$$

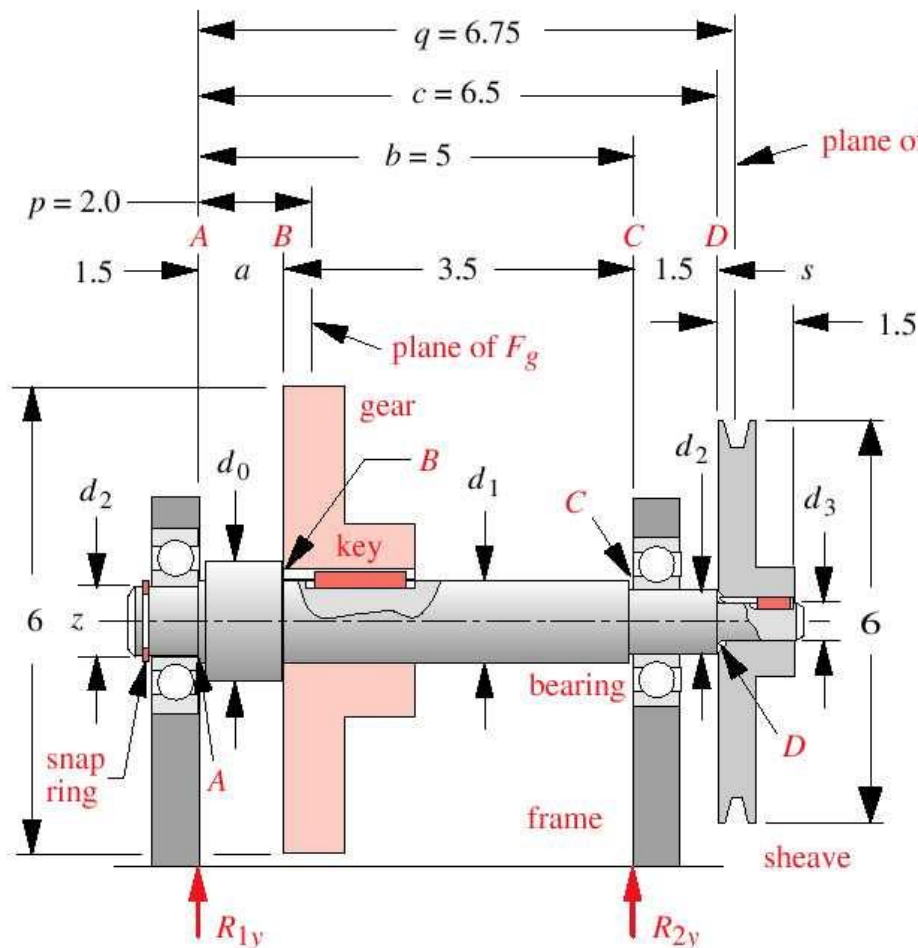


Shaft design

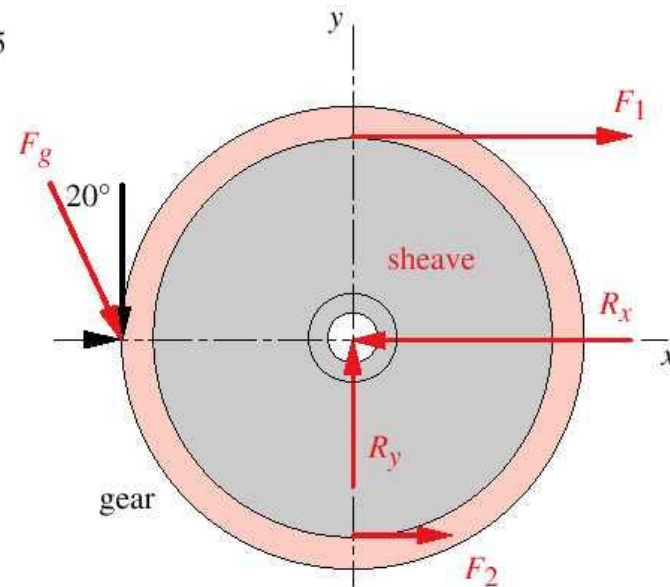
Fluctuating bending and torsion

Review and Master: Example 10-2

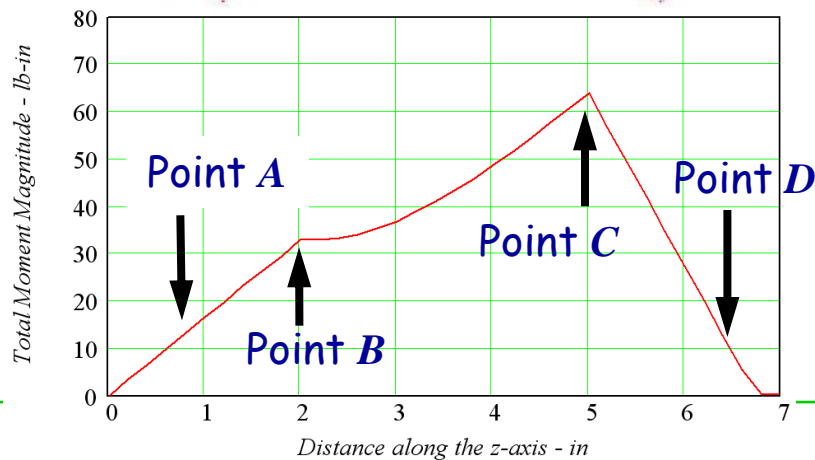
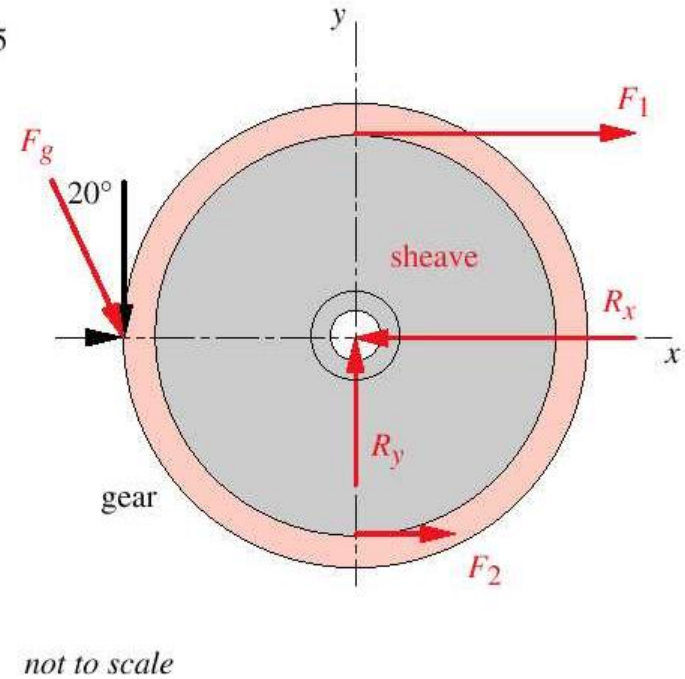
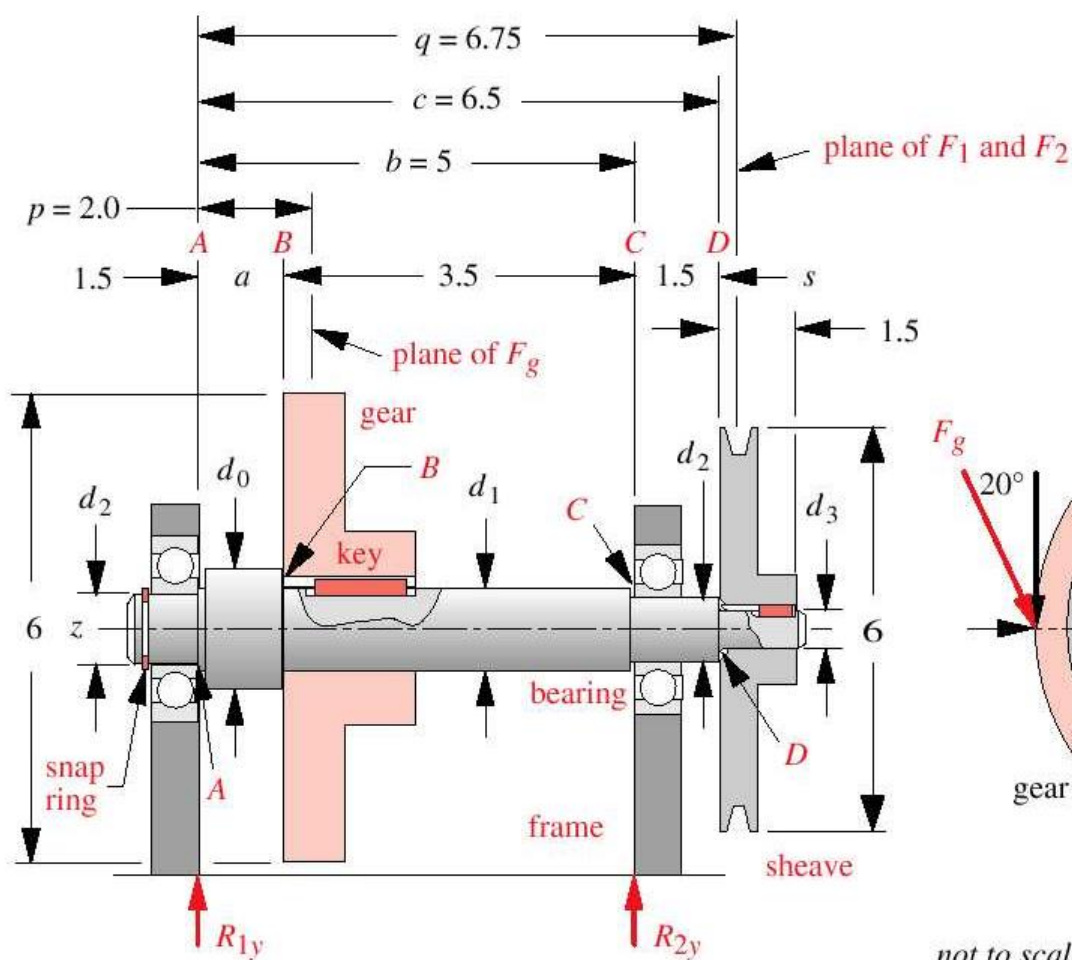
Design shaft to support attachments



- Mean and alternating torque are both 74 lb-in
- Safety factor: 2.5
- Infinite life
- Material: SAE 1020 (good notch sensitivity)
- Operating conditions: room temperature
- Power: 2 HP at 1,750 rpm
- SCF of 3.5 for radii in bending, 2 in torsion, and 4 at the keyway



not to scale



Total moment:

$$M_T(z) = \left[M_{X-Z}^2 + M_{Y-Z}^2 \right]^{1/2}$$



Shaft design

ASME method: fully-reversed bending and constant torsion

- Based on failure envelope (shown before):

$$\left(\frac{\sigma_a}{S_e}\right)^2 + \left(\frac{\tau_m}{S_{ys}}\right)^2 = 1$$

- Safety factor: N_f

- von Mises stress in shear (strain-energy theory): $S_{ys} = \frac{S_y}{\sqrt{3}}$

- Amplitude stress in bending and mean torsional stresses: σ_a, τ_m
(corrected for fatigue stress-concentration factors)

- Shaft diameter is calculated as:

$$d = \left\{ \frac{32N_f}{\pi} \left[\left(K_f \frac{M_a}{S_f} \right)^2 + \frac{3}{4} \left(K_{fsm} \frac{T_m}{S_y} \right)^2 \right]^{1/2} \right\}^{1/3}$$



Shaft design

ASME method: fluctuating bending and torsion

□ Based on von Mises stresses (amplitude and mean): σ'_a, σ'_m

□ Failure envelope given as:

$$\frac{1}{N_f} = \frac{\sigma'_a}{S_f} + \frac{\sigma'_m}{S_{ut}}$$

□ von Mises stress in shear (strain-energy theory): $S_{ys} = \frac{S_y}{\sqrt{3}}$

□ Amplitude and mean stress components in bending and shear:
(corrected for fatigue stress-concentration factors) $\sigma_a, \sigma_m, \tau_a, \tau_m$

□ Shaft diameter is calculated as:

$$d = \left\{ \frac{32N_f}{\pi} \left[\frac{\sqrt{(K_f M_a)^2 + \frac{3}{4}(K_{fs} T_a)^2}}{S_f} + \frac{\sqrt{(K_{fm} M_m)^2 + \frac{3}{4}(K_{fsm} T_m)^2}}{S_{ut}} \right] \right\}^{1/3}$$



Shaft design

Deflection: bending

- Simple shafts: refer to notes from previous lectures
- Stepped shafts: *calculations become more involved*

$$\frac{M}{EI} = \frac{\text{Moment function determined using singularity functions}}{EI}$$

It is required the
integration of equations:

$$\theta_{slope} = \int \frac{M}{EI} dz + C_3$$

$$\delta_{deflection} = \int \theta_{slope} dz + zC_3 + C_4$$

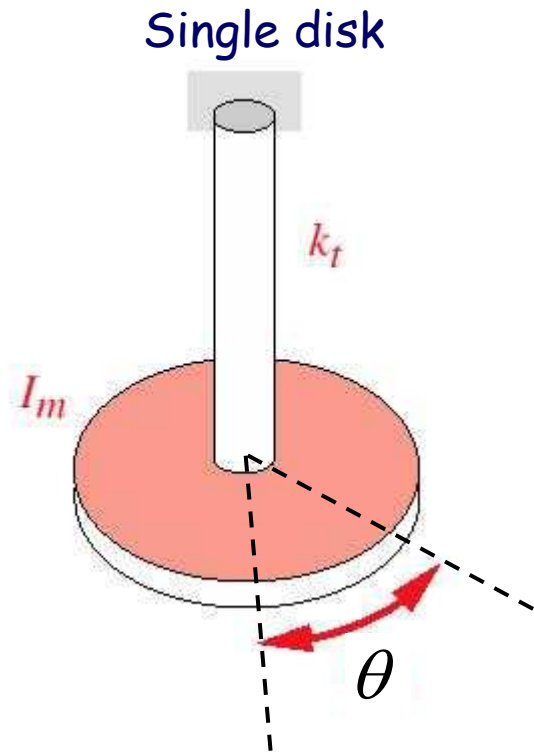
Numerical integration is preferred:

see MathCad Examples EX10-03 and EX10-09



Shaft design

Deflection: torsion



Angular deflection (simple shaft):

$$\theta = \frac{T l}{G J}$$

Torsional spring constant (simple shaft):

$$k_t = \frac{T}{\theta} = \frac{G J}{l}$$

Angular deflection (stepped shaft):

$$\theta = \theta_1 + \theta_2 + \theta_3 = \frac{T}{G} \left(\frac{l_1}{J_1} + \frac{l_2}{J_2} + \frac{l_3}{J_3} \right)$$

Effective torsional spring constant (stepped shaft):

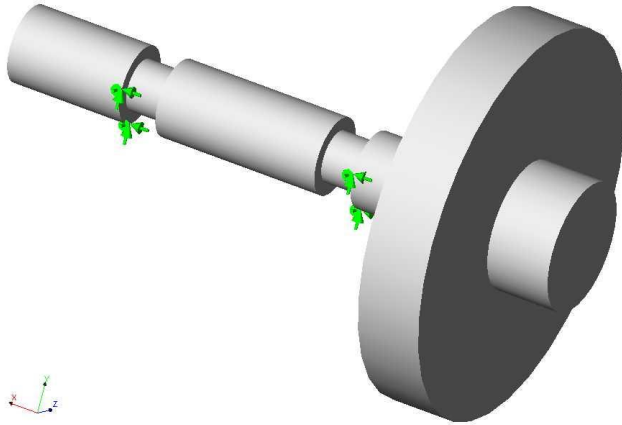
$$\frac{1}{k_{t_{\text{effective}}}} = \frac{1}{k_{t_1}} + \frac{1}{k_{t_2}} + \frac{1}{k_{t_3}}$$



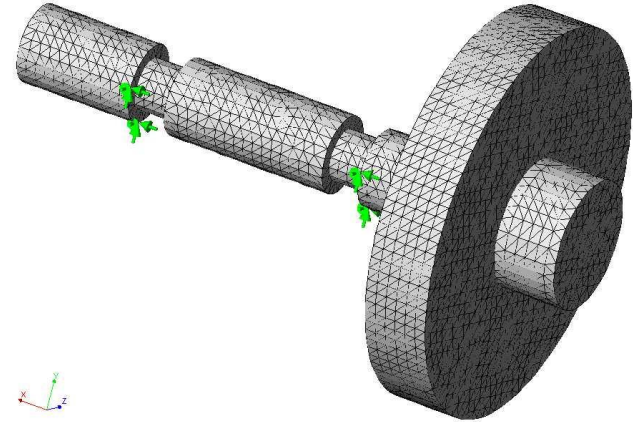
Shaft design

Natural frequencies of vibration: FEM model of gear-shaft

CAD model



Domain discretization



Material

Select material source

Input

Center library

Library files

coswkm.lib

Steel

- Alloy Steel
- Cast Alloy Steel
- Cast Stainless S
- Plain Carbon St
- Cast Carbon St
- AISI 1020**
- AISI 304
- Stainless Steel i
- Wrought Stainle
- Iron

Material model

Type: Linear Elastic Isotropic

Use stress strain curve

Use large strain formulation

Use large displacement formulation

Updated Lagrangian Total Lagrangian

Property	Description	Value	Units	Temp. Curve
EX	Elasticity modulus (1st di	2e+011	N/m^2	←
NUXY	Poisson's ratio in XY dir	0.29	NA	←
GXY	Shear modulus in XY dir	7.7e+010	N/m^2	←
DENS	Mass Density	7900	kg/m^3	←
SIGXT	Tensile strength (X dir)	4.20507e+008	N/m^2	
SIGXC	Compressive strength (X		N/m^2	
SIGYLD	Yield stress	3.51571e+008	N/m^2	
ALPX	Coeff. of thermal expansi	1.5e-005	/Kelvin	
KX	Thermal conductivity (X-	47	W/(m.K)	
C	Specific heat	420	J/(kg.K)	

FEM model solves the discrete version of equation:

$$\sum F = m \ddot{x}$$

Also written as

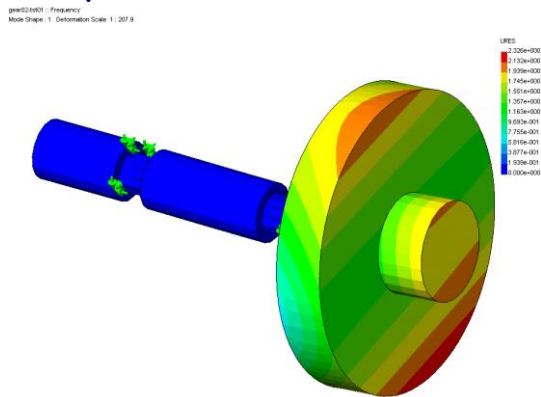
$$m \ddot{x} + k x = 0$$

Shaft design

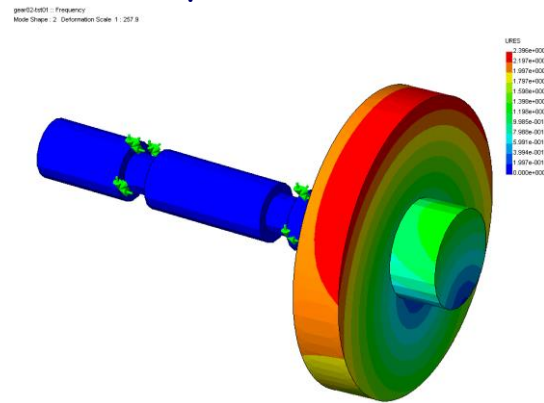
Natural frequencies of vibration: FEM model of gear-shaft

Representative results

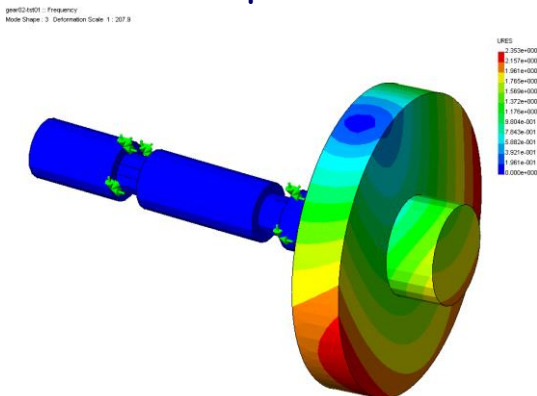
Mode shape #1 (fundamental) ~ 1040 Hz



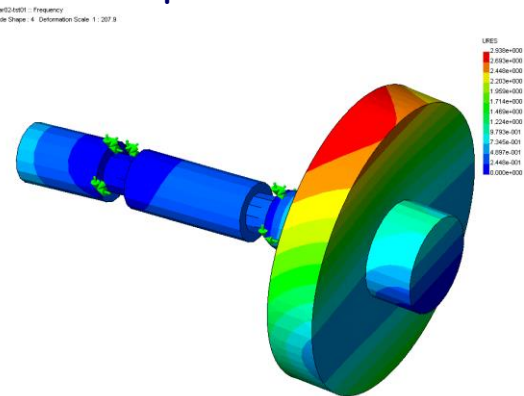
Mode shape #2 ~ 1240 Hz



Mode shape #3 ~ 1340 Hz

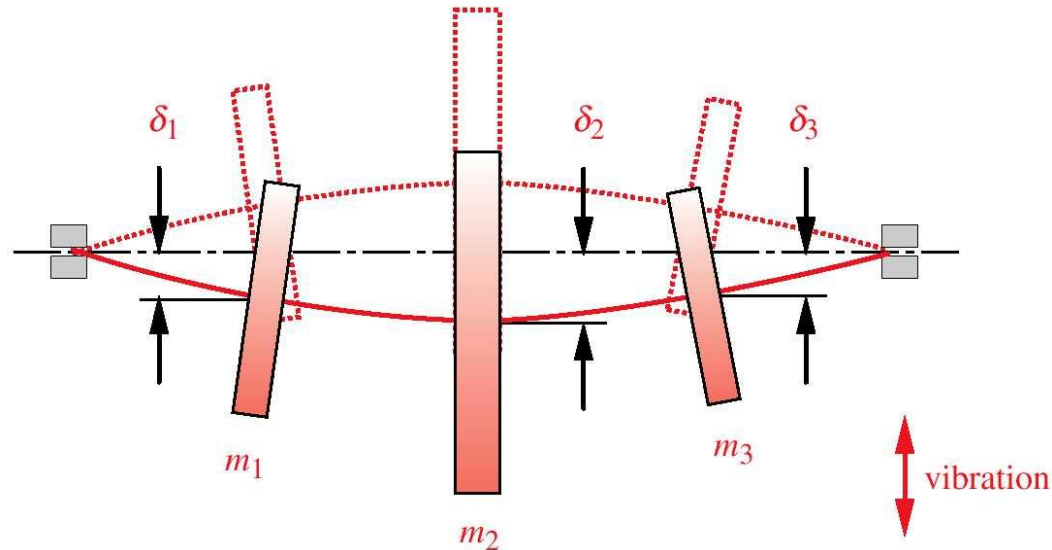


Mode shape #4 ~ 5320 Hz



Shaft design: transversal modes of vibration

Estimation of fundamental transversal first natural frequency

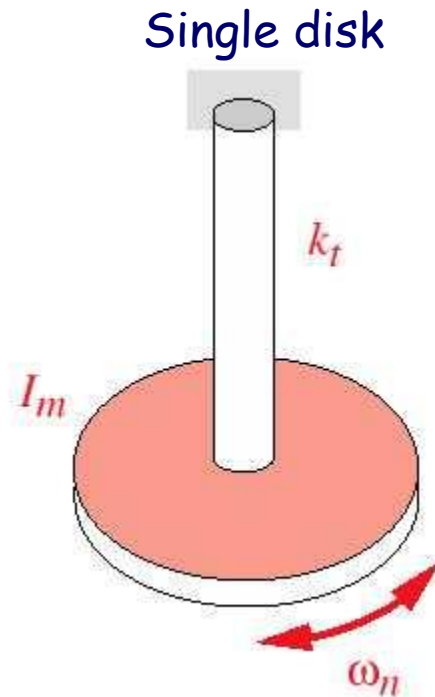


Using Rayleigh's method:
$$\omega_n = \sqrt{g \frac{\sum_i m_i \delta_i}{\sum_i m_i \delta_i^2}} ; [\text{rad/sec}]$$



Shaft design: torsional modes of vibration

Estimation of fundamental torsional first natural frequency



Simple shaft: $\omega_n = \sqrt{\frac{k_t}{I_m}}$

With: $k_t = \frac{GJ}{l}$, and $I_m = \frac{m r^2}{2}$

For stepped shafts:

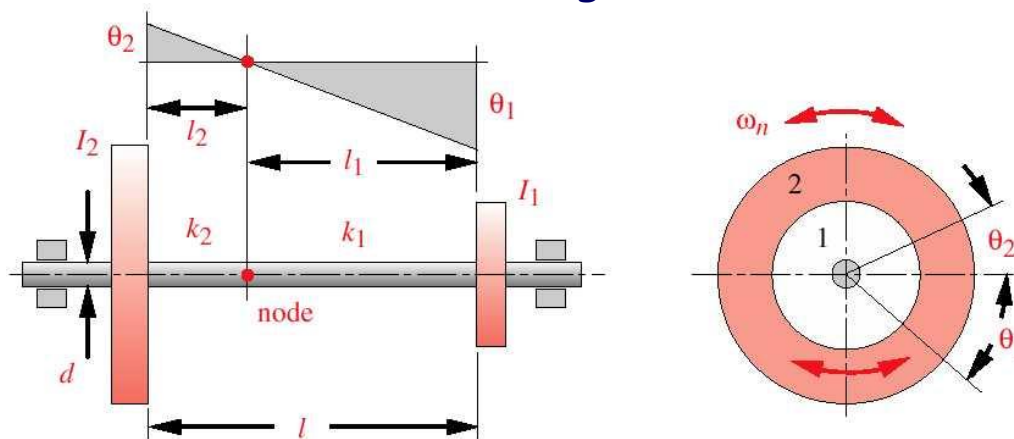
$$J = J_{eff} = \frac{l}{\sum_i \frac{l_i}{J_i}}$$



Shaft design: torsional modes of vibration

Estimation of fundamental torsional first natural frequency

Two disks configuration



Natural frequency:

$$\omega_n = \sqrt{k_{t_{effective}} \frac{I_1 + I_2}{I_1 I_2}}$$

Note that:

- 1) I_1 , and I_2 are mass moment of inertia
- 2) Effective torsional stiffness is

$$\frac{1}{k_{t_{effective}}} = \frac{1}{k_{t_1}} + \frac{1}{k_{t_2}}$$

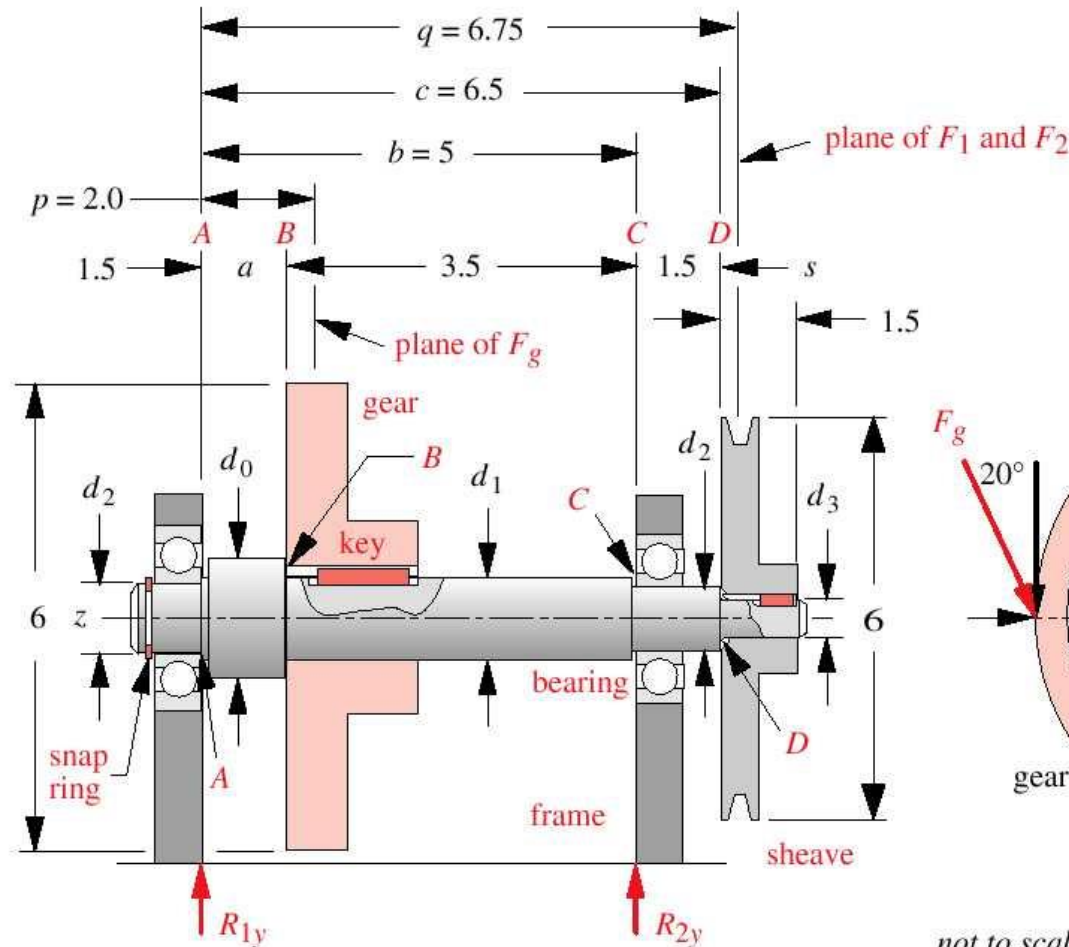
(when two ϕ steps define shaft geometry)



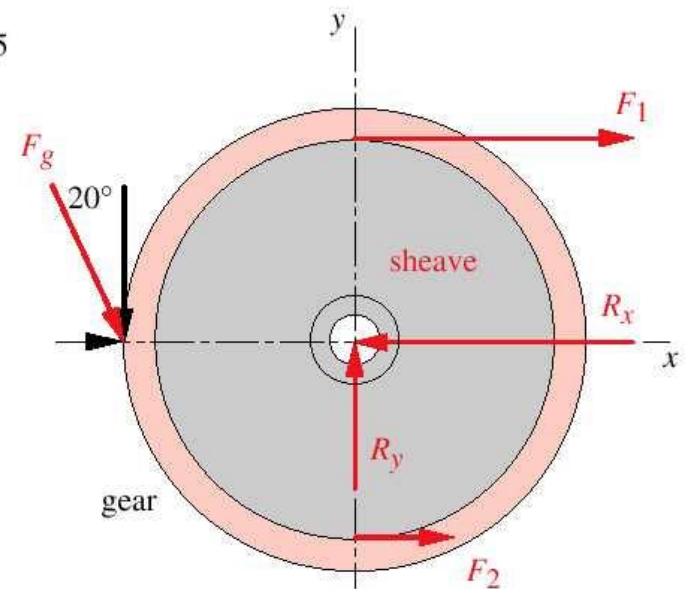
Shaft design: transversal & torsional modes of vibration

Example

□ Review and Master: Example 10-8



Requires use of numerical integration to find deflections at gear and sheave locations



not to scale



Reading

- Chapters 10 of textbook: Sections 10.9 to 10.16
- Review notes and text: ES2501, ES2502, ES2503

Homework assignment

- Author's: as indicated in website of our course
- Solve: as indicated in website of our course

