

# WORCESTER POLYTECHNIC INSTITUTE MECHANICAL ENGINEERING DEPARTMENT

## DESIGN OF MACHINE ELEMENTS ME-3320, B'2024

Lecture 05

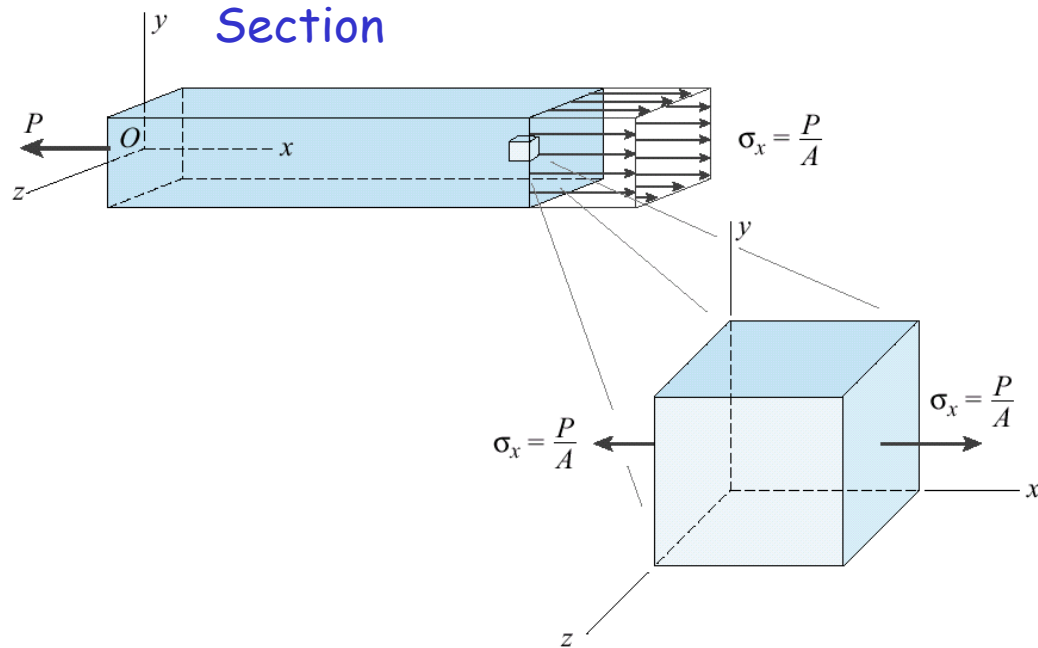
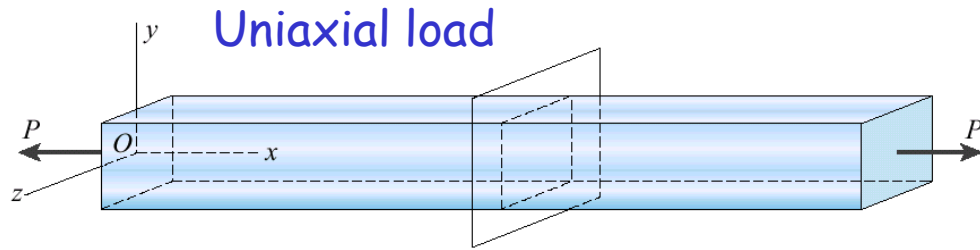
October 2024

Optional



# Stress at a point

## Uniaxial load

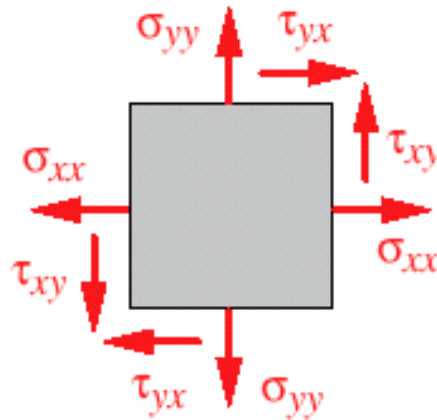
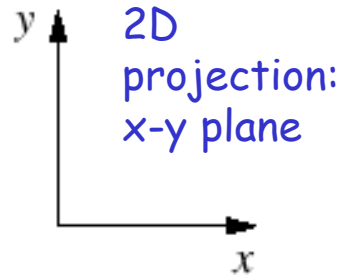


Stress cube  
for uniaxial  
stress  
loading



# Stress at a point

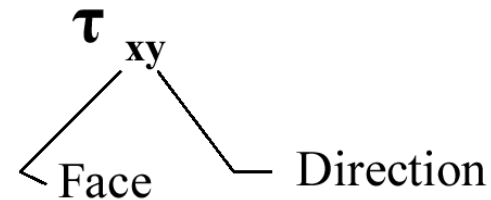
## General load case. Stress cube in 2D



### Notation

$\sigma$  Normal Stress

$\tau$  Shear Stress



Equilibrium conditions require that

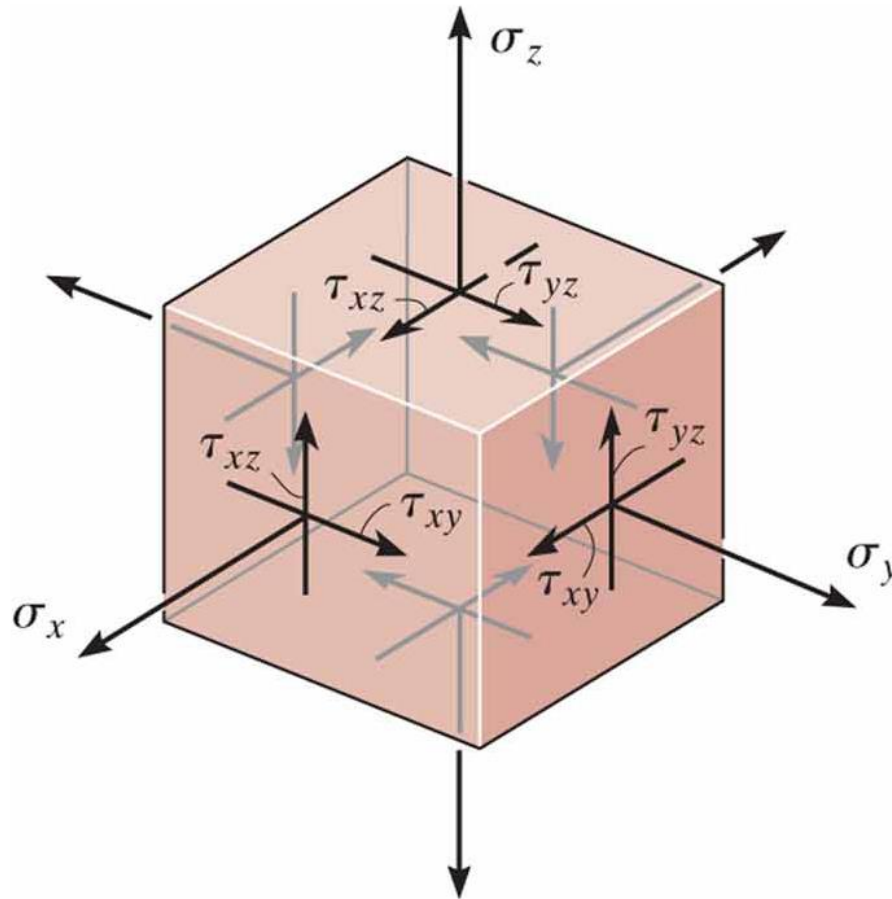
$$\tau_{xy} = \tau_{yx}$$

Why?



# Stress at a point

## General load case. Stress cube in 3D



There are 9 components of stress.

*Equilibrium conditions are used to reduce the number of stress components to 6:*

$$\tau_{xy} = \tau_{yx}$$

$$\tau_{xz} = \tau_{zx}$$

$$\tau_{yz} = \tau_{zy}$$

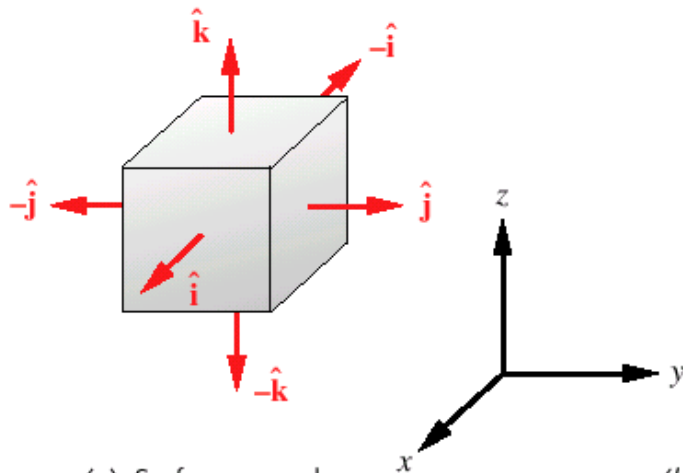


# Stress tensor

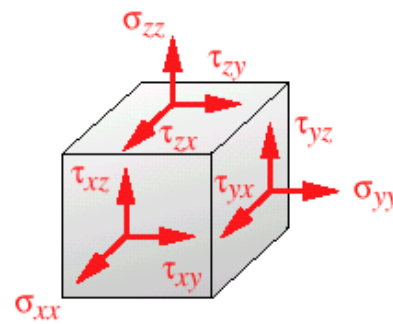
## Cauchy stress tensor

$$\begin{bmatrix} \sigma_{xx} & \tau_{xy} & \tau_{xz} \\ \tau_{yx} & \sigma_{yy} & \tau_{yz} \\ \tau_{zx} & \tau_{zy} & \sigma_{zz} \end{bmatrix}$$

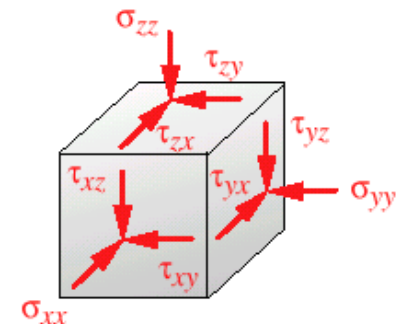
Tensors are quantities that are *invariant* to coordinate transformations



(a) Surface normals



(b) Positive stress components



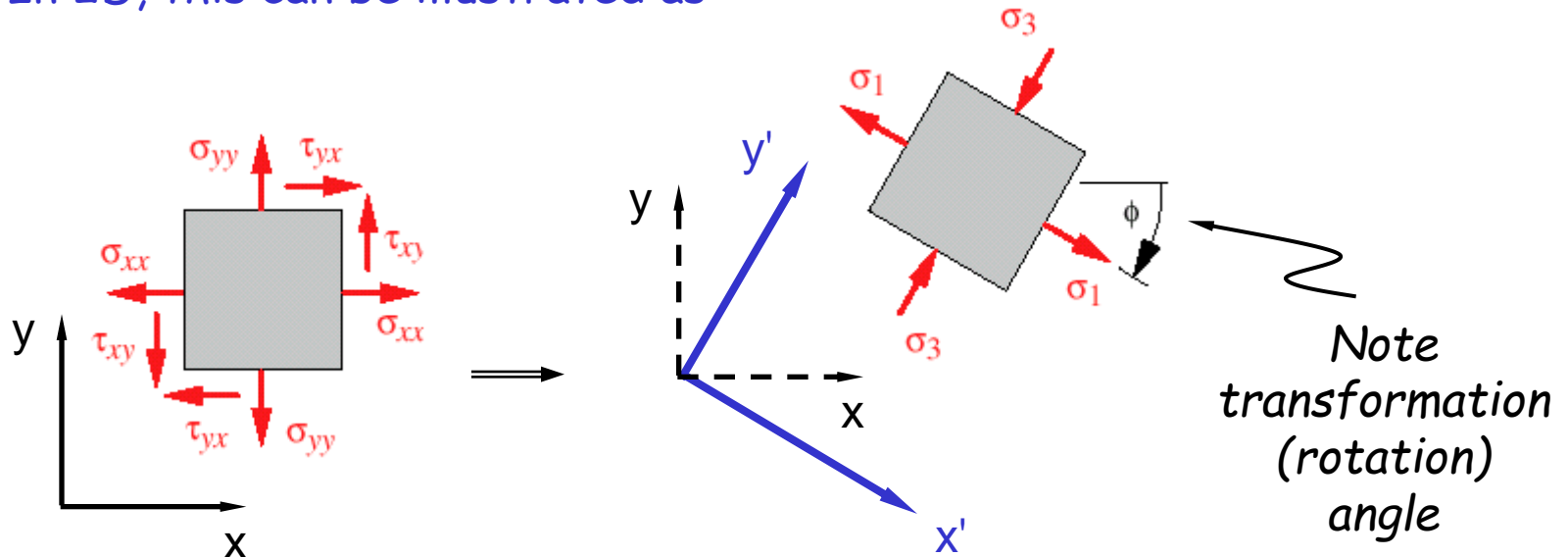
(c) Negative stress components



# Determination of principal stresses

## Principal normal stresses

- This problem involves performing coordinate transformation, which can provide a stress tensor that does NOT contain shear stresses
- In 2D, this can be illustrated as



Stress cube in original coordinate system  $(x, y)$

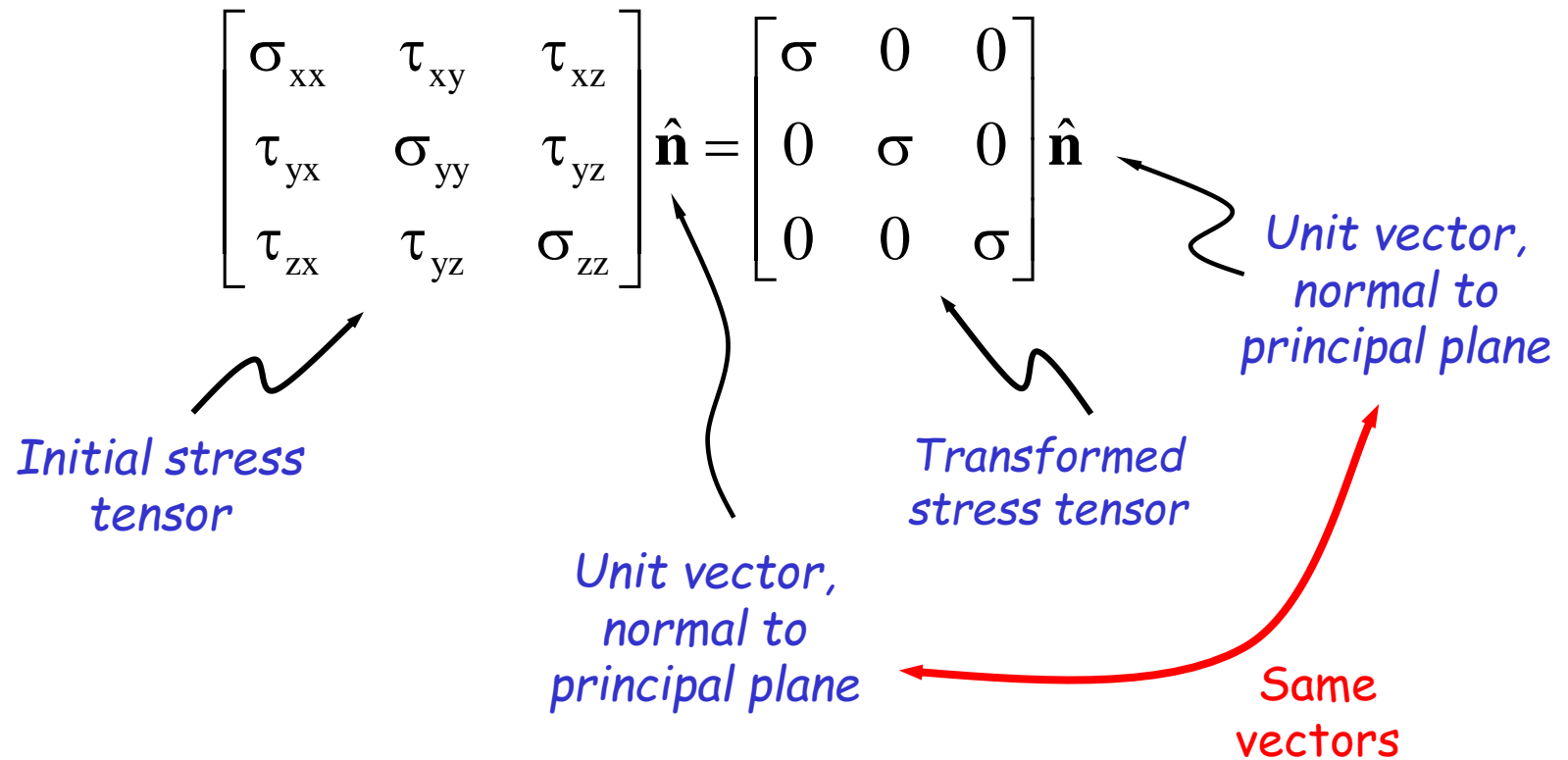
Stress cube in transformed coordinate system  $(x', y')$  -- only normal stresses exist:  $\sigma_1$  and  $\sigma_3$ , in this 2D case



# Determination of principal stresses

## Principal normal stresses

This problem involves performing coordinate transformation, which can provide a stress tensor that does NOT contain shear stresses, that is



# Determination of principal stresses

## Principal normal stresses

Previous equation can be written as

$$\begin{bmatrix} \sigma_{xx} - \sigma & \tau_{xy} & \tau_{xz} \\ \tau_{yx} & \sigma_{yy} - \sigma & \tau_{yz} \\ \tau_{zx} & \tau_{yz} & \sigma_{zz} - \sigma \end{bmatrix} \hat{\mathbf{n}} = \begin{bmatrix} \sigma_{xx} - \sigma & \tau_{xy} & \tau_{xz} \\ \tau_{yx} & \sigma_{yy} - \sigma & \tau_{yz} \\ \tau_{zx} & \tau_{yz} & \sigma_{zz} - \sigma \end{bmatrix} \begin{pmatrix} n_x \\ n_y \\ n_z \end{pmatrix} = \begin{pmatrix} 0 \\ 0 \\ 0 \end{pmatrix}$$

implying that the determinant

$$\begin{vmatrix} \sigma_{xx} - \sigma & \tau_{xy} & \tau_{xz} \\ \tau_{yx} & \sigma_{yy} - \sigma & \tau_{yz} \\ \tau_{zx} & \tau_{yz} & \sigma_{zz} - \sigma \end{vmatrix} = 0$$

(this is an Eigenvalue problem)





# Determination of principal stresses

## Principal normal stresses

Expanding determinant and setting it to zero yields

$$\sigma^3 - C_2\sigma^2 + C_1\sigma - C_0 = 0$$

in which

$$C_2 = \sigma_{xx} + \sigma_{yy} + \sigma_{zz}$$

$$C_1 = \sigma_{xx}\sigma_{yy} + \sigma_{yy}\sigma_{zz} + \sigma_{zz}\sigma_{xx} - \tau_{xy}^2 - \tau_{yz}^2 - \tau_{zx}^2$$

$$C_0 = \sigma_{xx}\sigma_{yy}\sigma_{zz} + 2\tau_{xy}\tau_{yz}\tau_{zx} - \sigma_{xx}\tau_{yz}^2 - \sigma_{yy}\tau_{zx}^2 - \sigma_{zz}\tau_{xy}^2$$

are stress invariants (have the same magnitudes for all choices of coordinate axes  $(x,y,z)$  in which the applied stresses are measured or calculated)

The principal normal stresses,  $\sigma_1, \sigma_2, \sigma_3$ , are the three roots of the cubic polynomial -- always real and typically ordered as:  $\sigma_1 > \sigma_2 > \sigma_3$



# Determination of principal stresses

## Principal shear stresses

Principal *shear stresses* can be found from values of the principal normal stresses as

$$\tau_{13} = \frac{|\sigma_1 - \sigma_3|}{2}$$

$$\tau_{21} = \frac{|\sigma_2 - \sigma_1|}{2}$$

$$\tau_{32} = \frac{|\sigma_3 - \sigma_2|}{2}$$



# Mohr's circle: principal normal and shear stresses

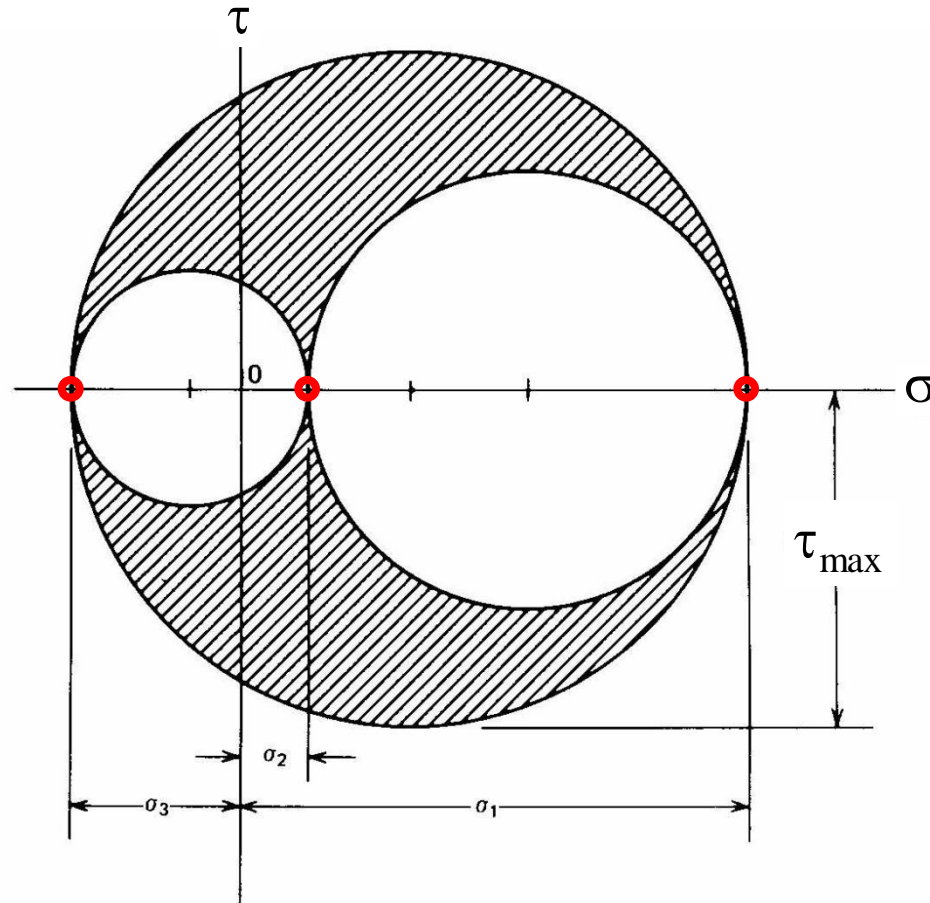
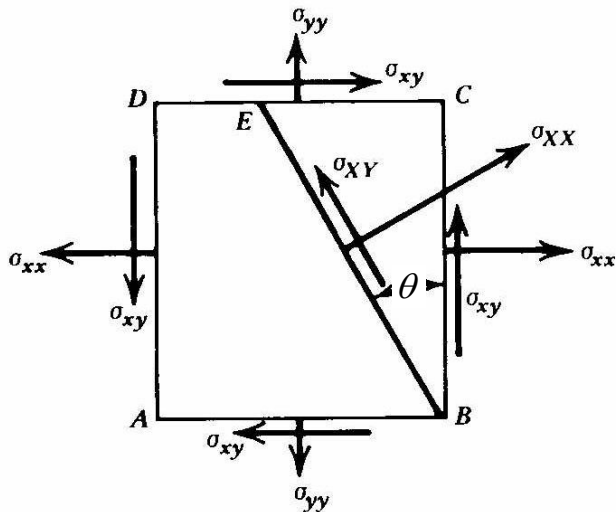
## Graphical representation of previous equations: 3D

Equivalent nomenclature:

$$\sigma_x = \sigma_{xx}$$

$$\sigma_y = \sigma_{yy}$$

$$\sigma_{xy} = \tau_{xy}$$



Mohr's Circle in three dimensions.  
From Boreis: *Mechanics of materials*



# Determination of principal stresses

## Principal normal and shear stresses: 2D case

We will use these equations extensively

Principal normal stresses:

$$\sigma_1, \sigma_3 = \frac{\sigma_{xx} + \sigma_{yy}}{2} \pm \sqrt{\left(\frac{\sigma_{xx} - \sigma_{yy}}{2}\right)^2 + \tau_{xy}^2}$$

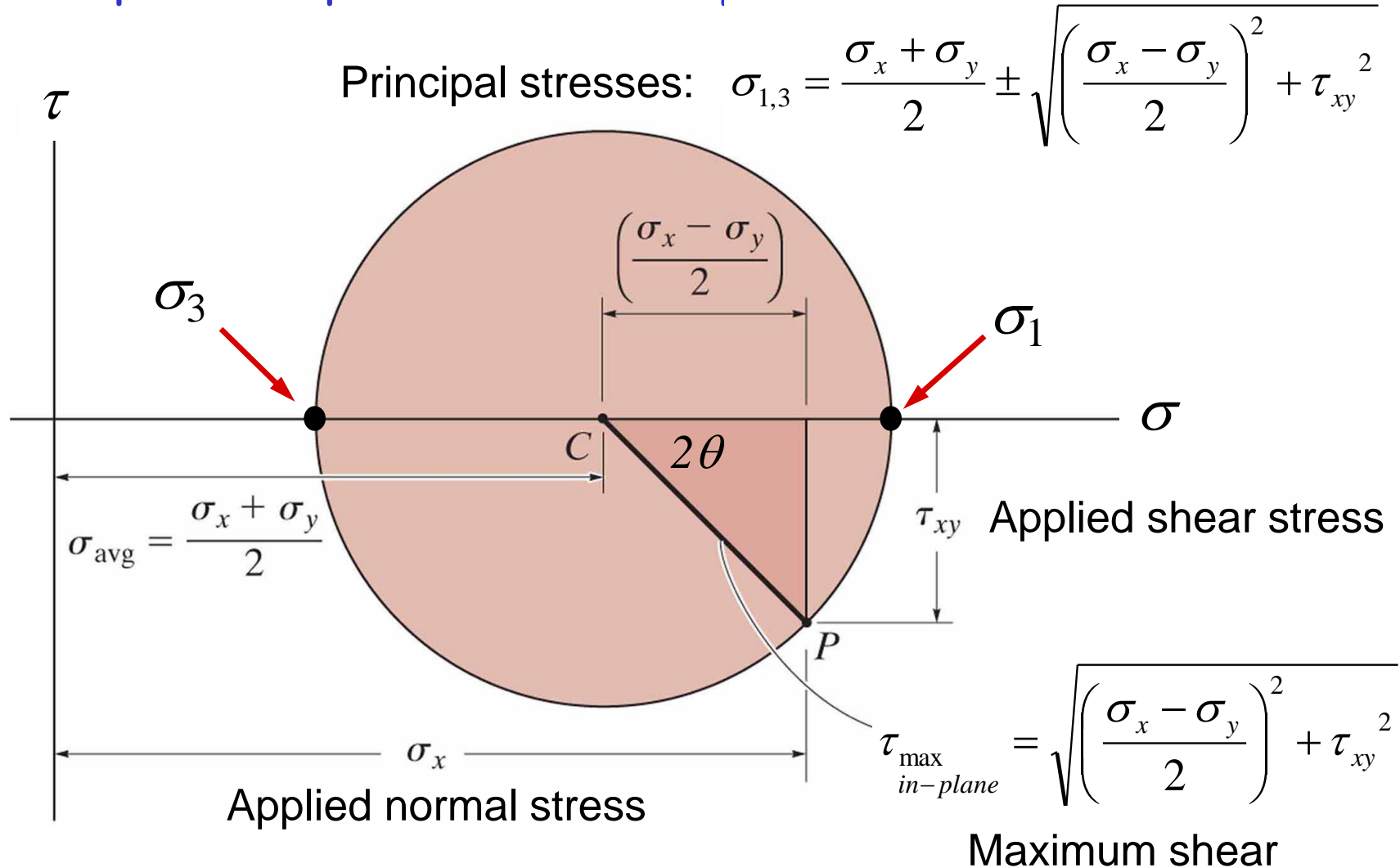
Maximum shear stress:

$$\tau_{\max} = \sqrt{\left(\frac{\sigma_{xx} - \sigma_{yy}}{2}\right)^2 + \tau_{xy}^2}$$



# Mohr's circle: principal normal and shear stresses

Graphical representation of previous equations: 2D



# Determination of principal stresses

## Review author's textbook

- Examples: 4-1, 4-2, and 4-3
- Review and master Section 4.6

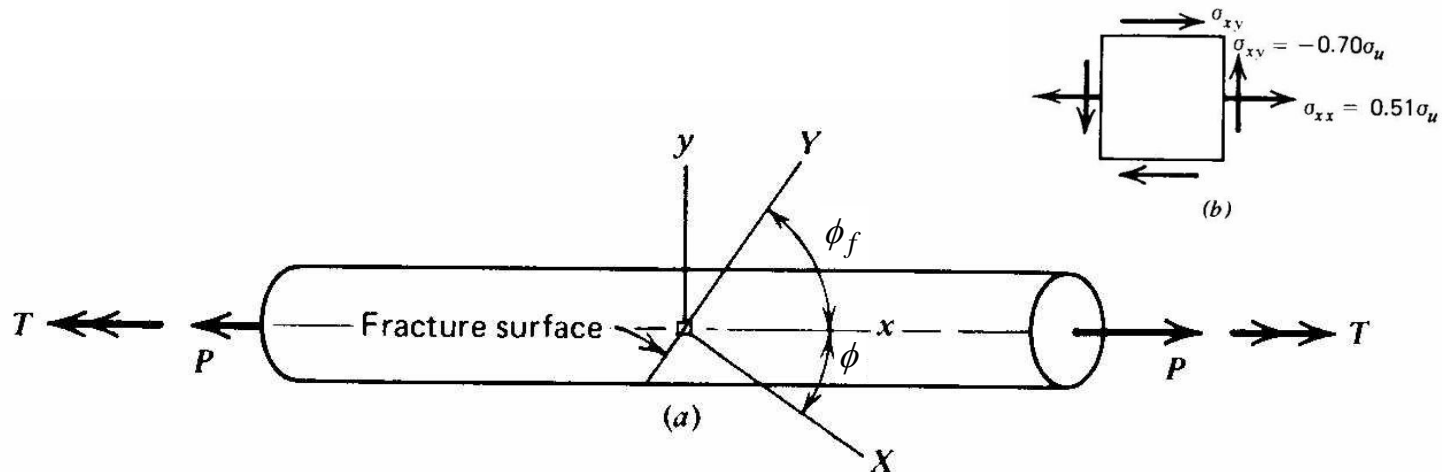


# Determination of principal stresses

## Example: solve in class / assignment

A piece of chalk is subjected to combined loading consisting of a tensile load  $P$  and a torque  $T$ , see figure. The chalk has an ultimate strength  $\sigma_u$  as determined by a tensile test. The load  $P$  remains constant at such a value that it produces a tensile test of  $0.51 \cdot \sigma_u$  on any cross-section. The torque  $T$  is increased gradually until fracture occurs on some inclined surface.

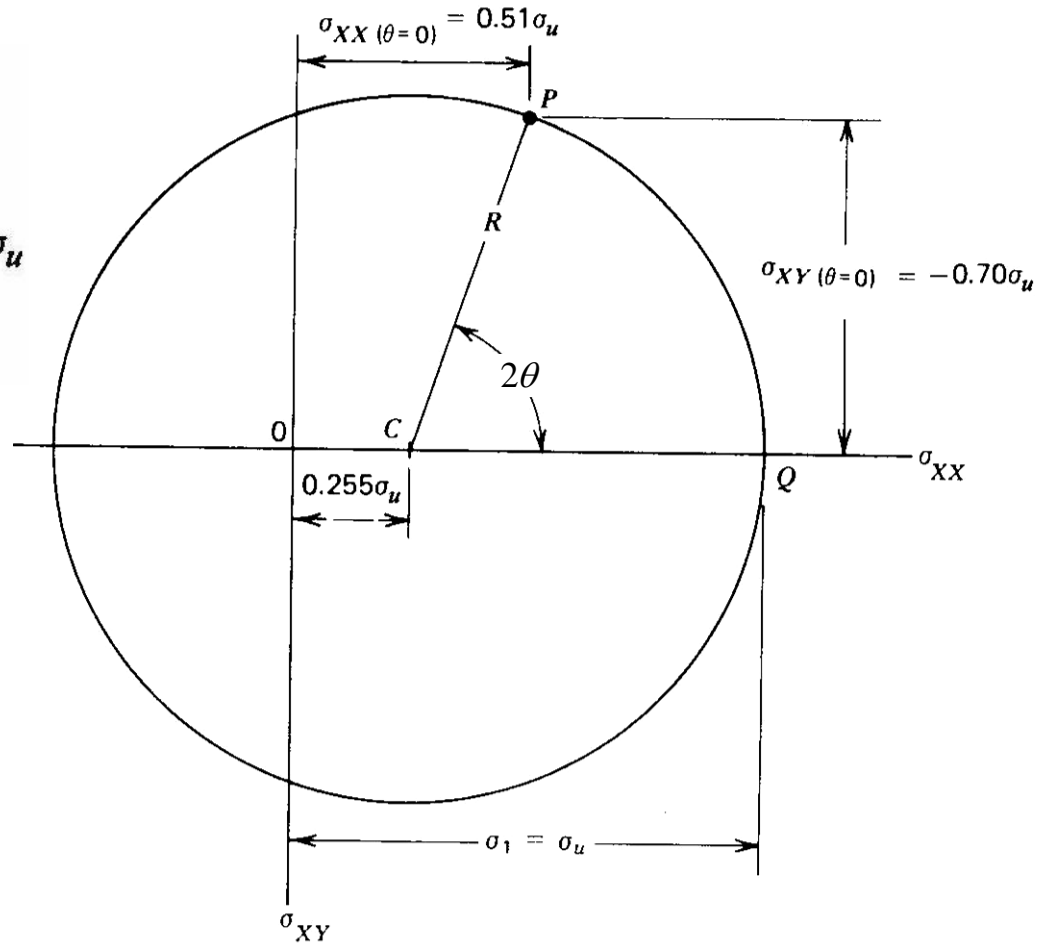
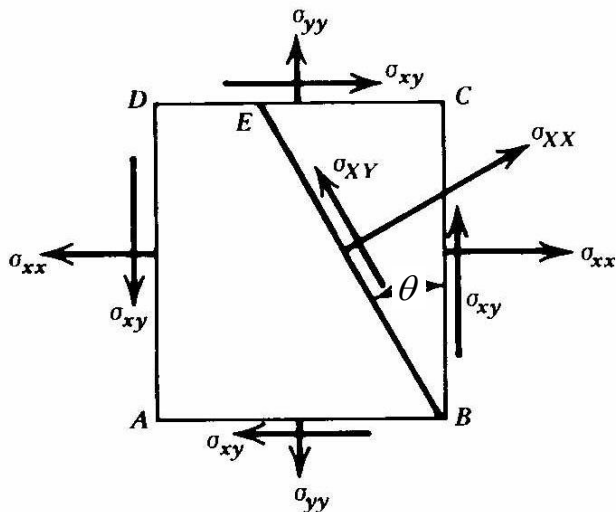
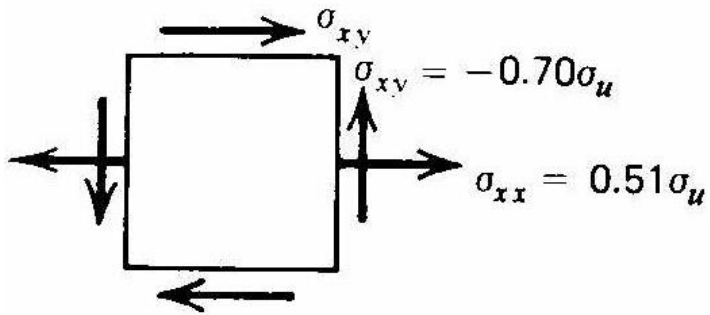
Assuming that fracture takes place when the maximum principal stress  $\sigma_1$  reaches the ultimate strength  $\sigma_u$ , **determine the magnitude of the torsional shearing stress produced by the torque  $T$  at fracture and determine the orientation of the fracture surface.**



# Determination of principal stresses

Example: solve in class / assignment

Stress element





# Reading assignment

- Chapters 4 of textbook: Sections 4.0 to 4.6
- Review notes and text: ES2501, ES2502

# Homework assignment

- **Author's:** as posted in Website of our course
- **Solve:** as posted in Website of our course

