

WORCESTER POLYTECHNIC INSTITUTE MECHANICAL ENGINEERING DEPARTMENT

STRESS ANALYSIS ES-2502, D'2020

We will get started soon...



12 May 2020



WORCESTER POLYTECHNIC INSTITUTE MECHANICAL ENGINEERING DEPARTMENT

STRESS ANALYSIS ES-2502, D'2020

We will get started soon...

Lecture 26:

Unit 24, 25:

Principal Stresses. Mohr's circle

12 May 2020



General information

Instructor: Cosme Furlong
HL-152
(774) 239-6971 - Texting Works

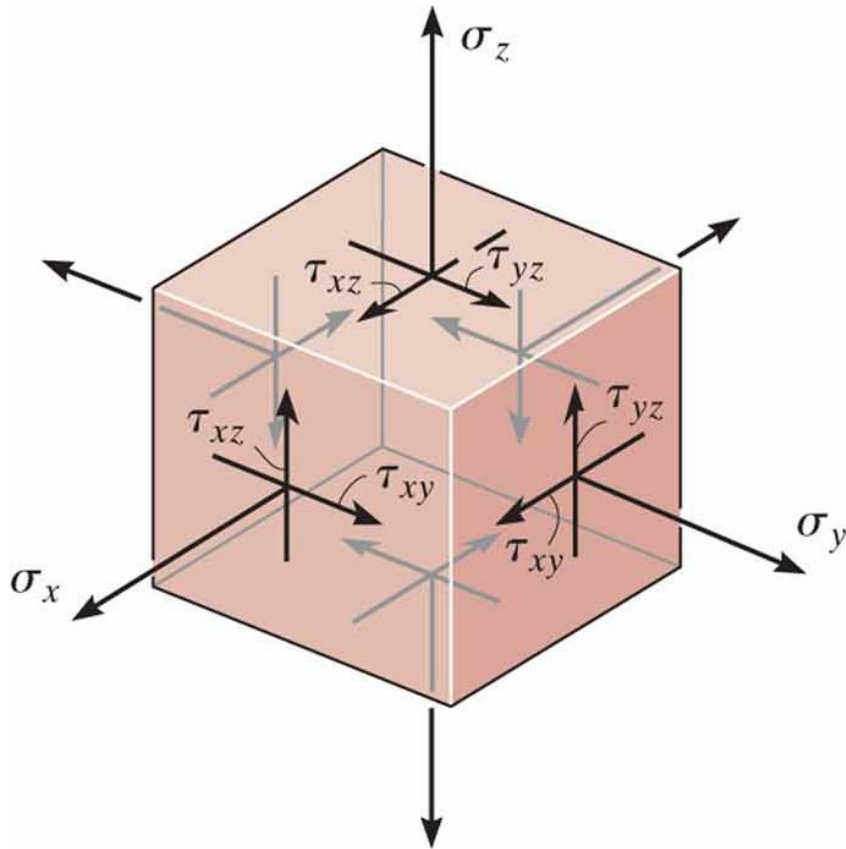
Email: cfurlong @ wpi.edu
<http://www.wpi.edu/~cfurlong/es2502.html>

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Stress at a point

General state of stress. Stress cube in 3D



Notation

σ Normal Stress

τ Shear Stress

τ_{xy}

Face Direction

Equilibrium conditions require that:

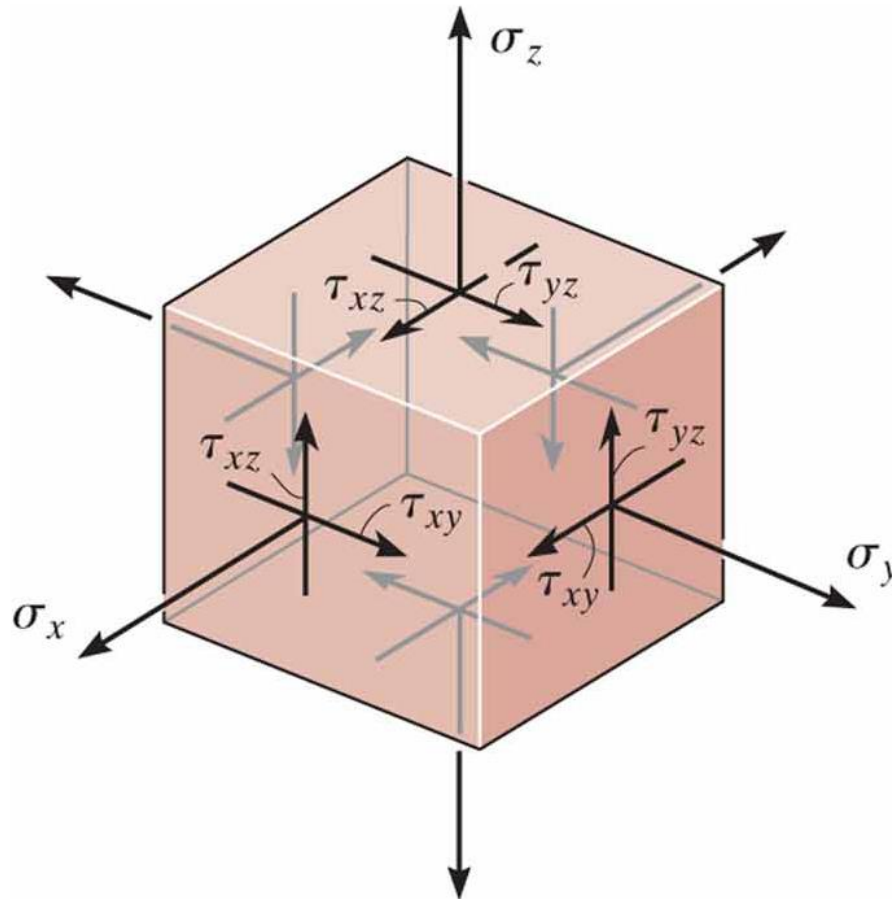
$$\tau_{xy} = \tau_{yx}, \tau_{xz} = \tau_{zx}, \tau_{yz} = \tau_{zy}$$

Why?



Stress at a point

General state of stress. Stress cube in 3D



There are 9 components of stress.

Equilibrium conditions are used to reduce the number of stress components to 6:

$$\tau_{xy} = \tau_{yx}$$

$$\tau_{xz} = \tau_{zx}$$

$$\tau_{yz} = \tau_{zy}$$

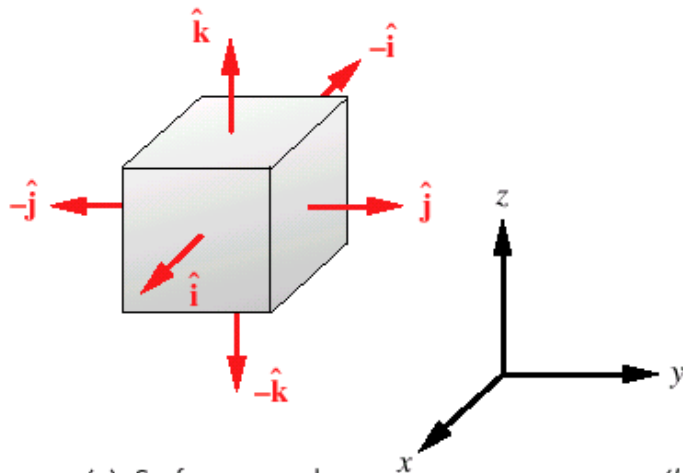


Stress tensor

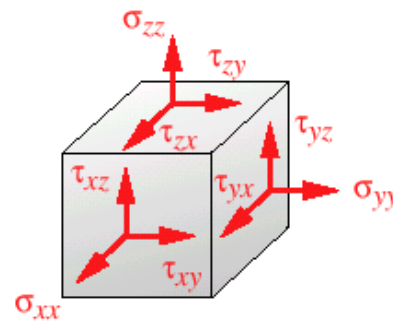
Cauchy stress tensor

$$\begin{bmatrix} \sigma_{xx} & \tau_{xy} & \tau_{xz} \\ \tau_{yx} & \sigma_{yy} & \tau_{yz} \\ \tau_{zx} & \tau_{zy} & \sigma_{zz} \end{bmatrix}$$

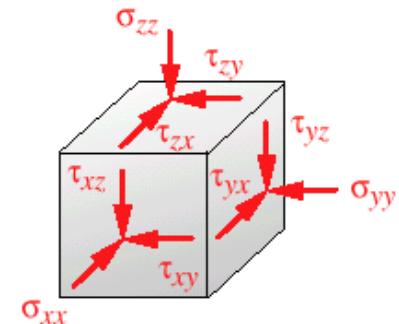
Tensors are quantities that are *invariant* to coordinate transformations (i.e., translations & rotations)



(a) Surface normals



(b) Positive stress components



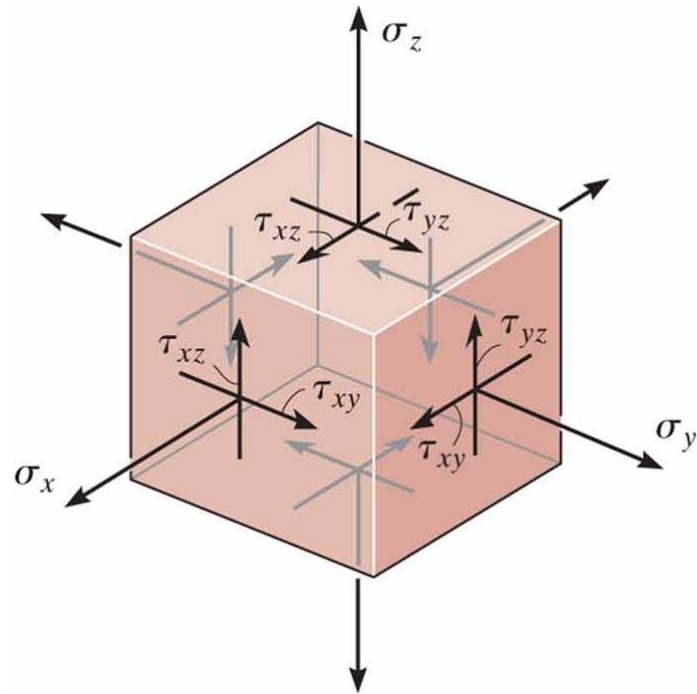
(c) Negative stress components



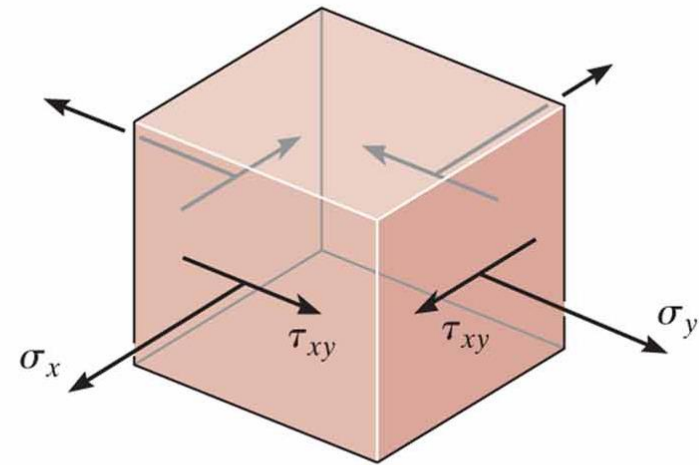
Stress at a point

Plane stress

General state of stress

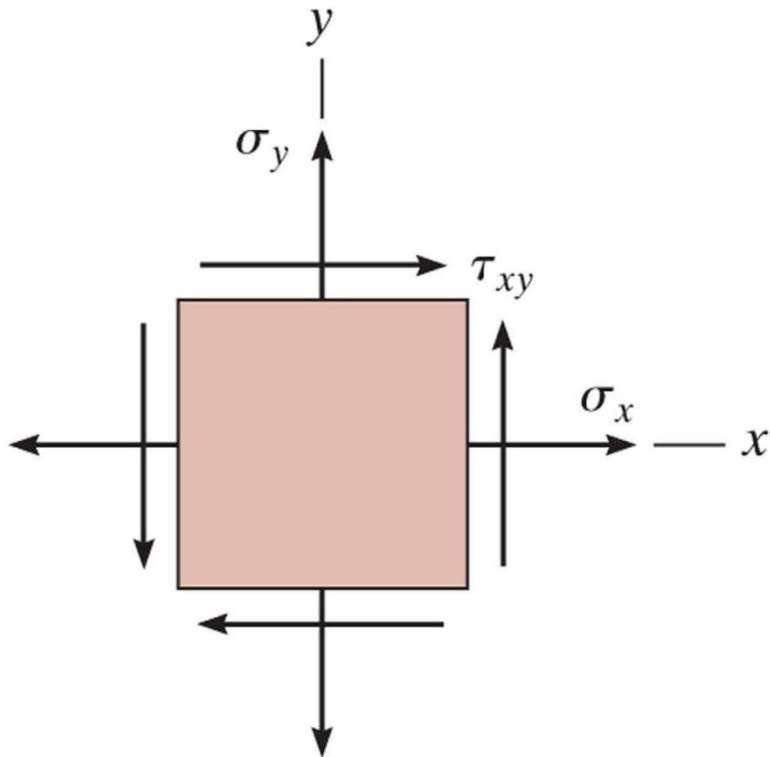


Plane stress

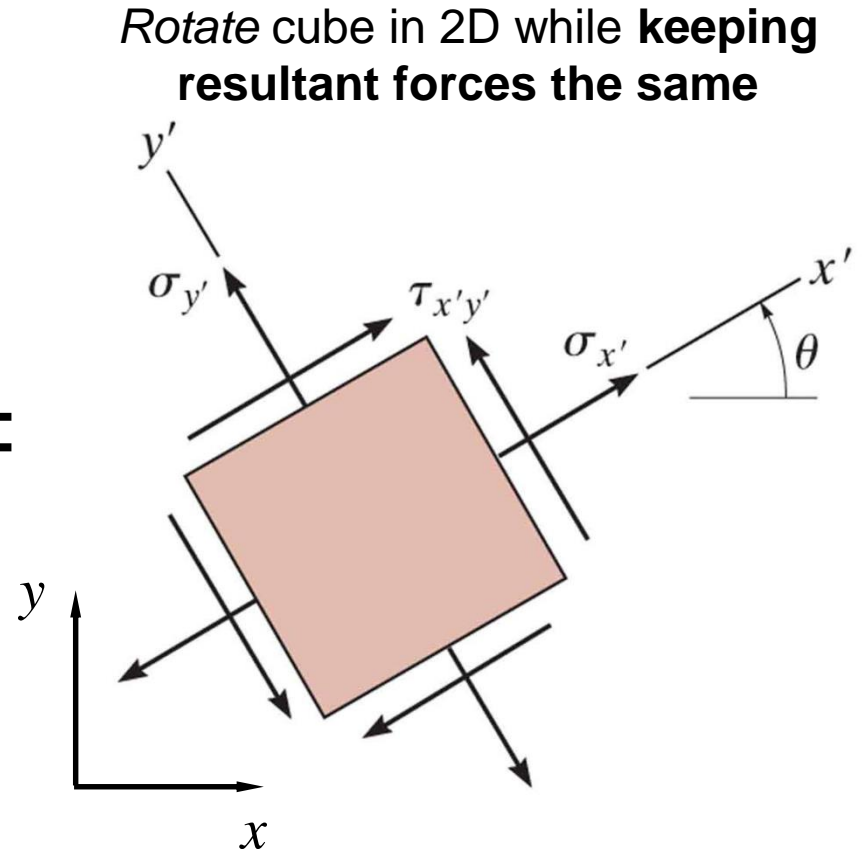


Plane stress transformation (rotation)

Stress cube in 2D

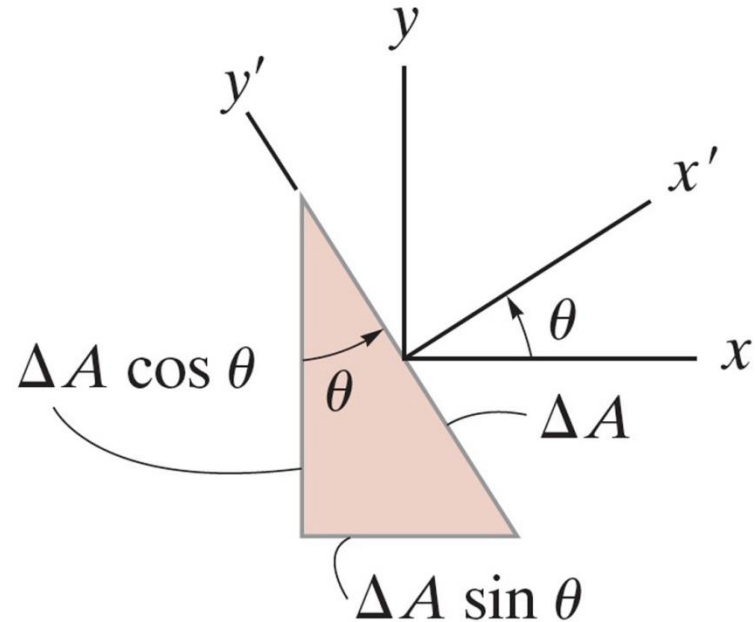
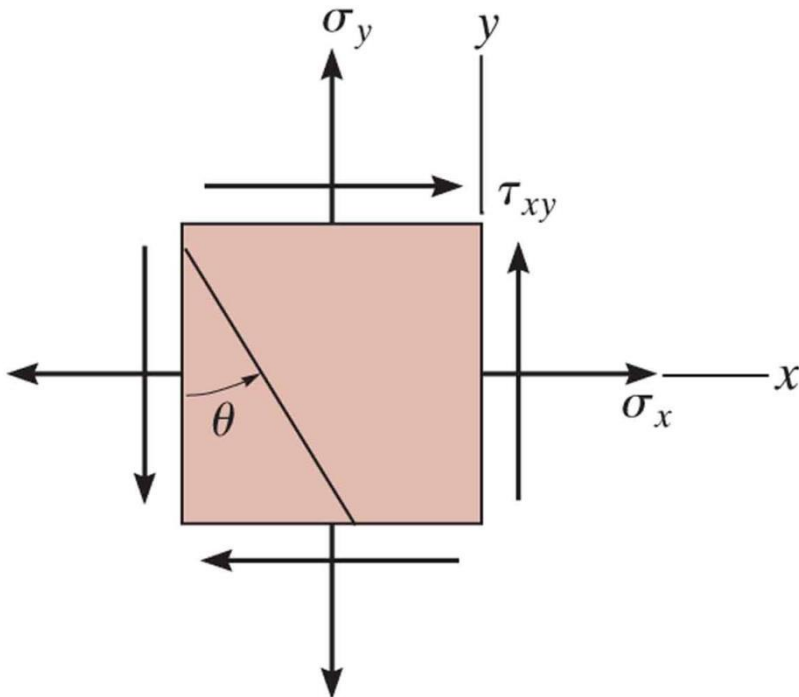


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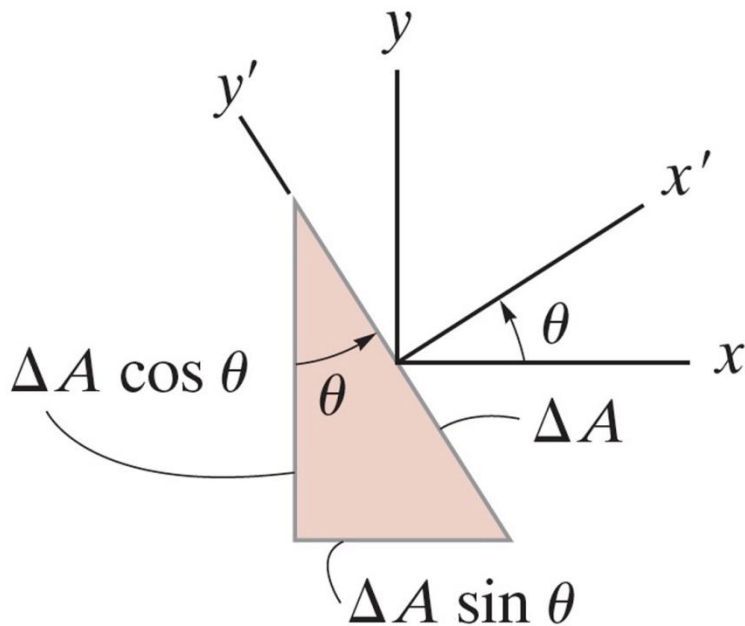
Plane stress transformation (rotation)

Introduce plane rotated at angle θ , therefore defining area ΔA

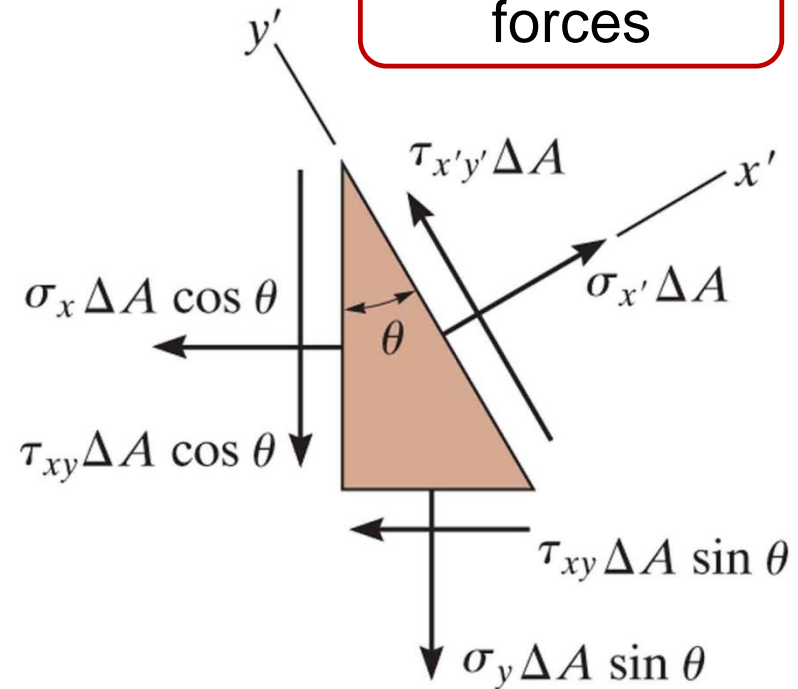


Plane stress transformation (rotation)

Plane rotated at angle θ defining area ΔA



Corresponding forces

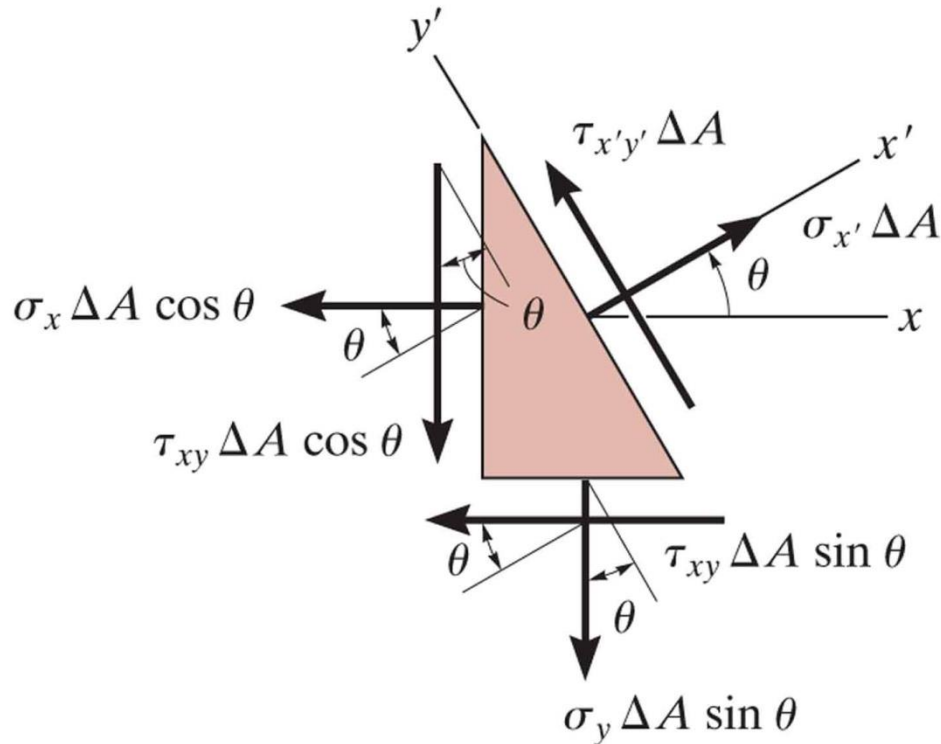


Plane stress transformation (rotation)

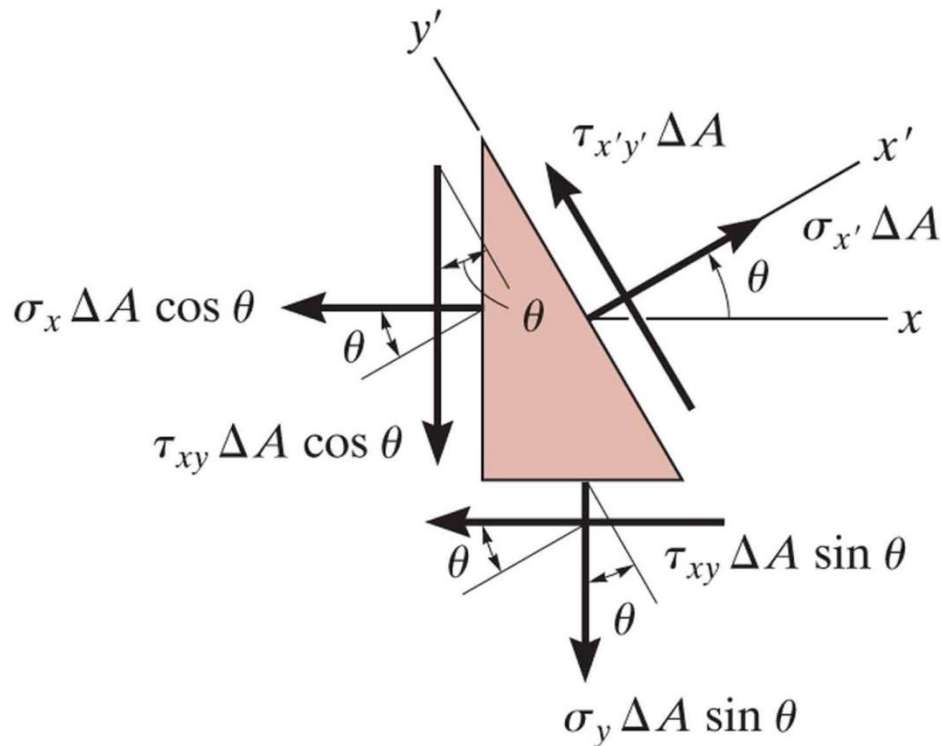
Apply equilibrium conditions:

$$(1) \quad \sum F_{x'} = 0; \quad + \nearrow$$

$$(2) \quad \sum F_{y'} = 0; \quad + \nwarrow$$



Plane stress transformation (rotation)



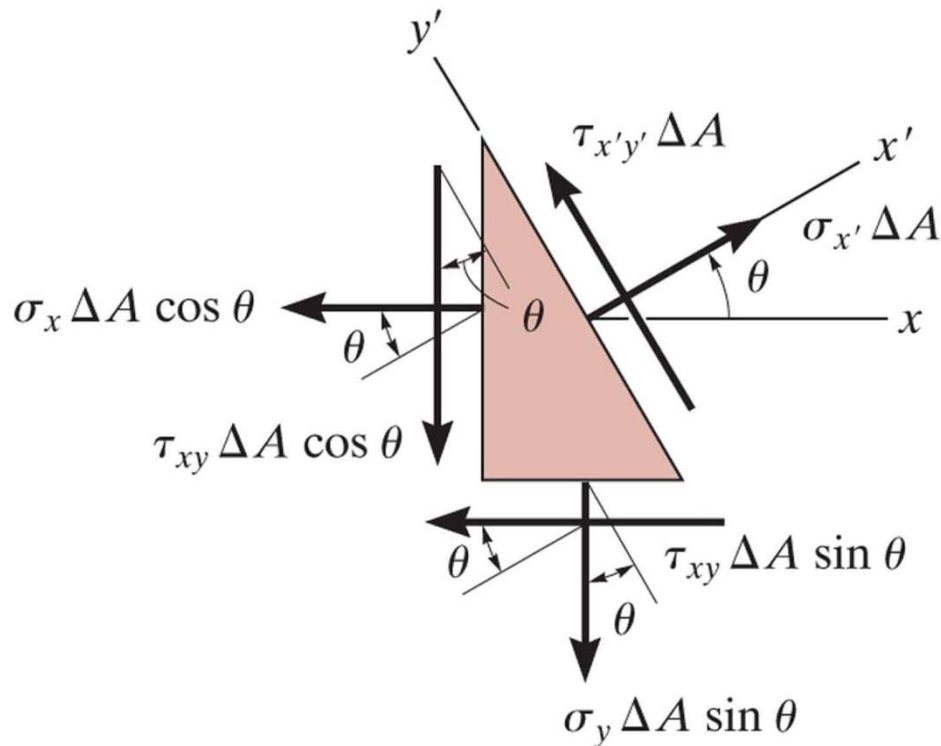
First equilibrium condition:

$$(1) \quad \sum F_{x'} = 0; \quad + \nearrow$$

$$\begin{aligned} & \sigma_{x'} \Delta A - (\tau_{xy} \Delta A \sin \theta) \cos \theta \\ & - (\sigma_y \Delta A \sin \theta) \sin \theta \\ & - (\tau_{xy} \Delta A \cos \theta) \sin \theta \\ & - (\sigma_x \Delta A \cos \theta) \cos \theta = 0 \end{aligned}$$



Plane stress transformation (rotation)



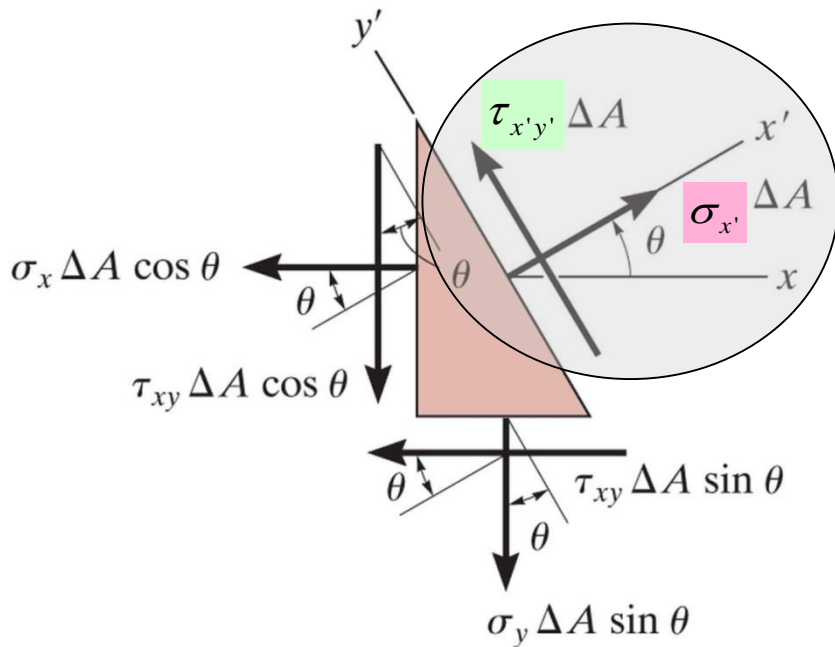
Second equilibrium condition:

$$(2) \quad \sum F_{y'} = 0; \quad + \nearrow$$

$$\begin{aligned} & \tau_{x'y'} \Delta A + (\tau_{xy} \Delta A \sin \theta) \sin \theta \\ & - (\sigma_y \Delta A \sin \theta) \cos \theta \\ & - (\tau_{xy} \Delta A \cos \theta) \cos \theta \\ & + (\sigma_x \Delta A \cos \theta) \sin \theta = 0 \end{aligned}$$



Plane stress transformation (rotation)



Transformation equations become:

$$\sigma_{x'} = \frac{\sigma_x + \sigma_y}{2} + \frac{\sigma_x - \sigma_y}{2} \cos 2\theta + \tau_{xy} \sin 2\theta$$

$$\tau_{x'y'} = -\frac{\sigma_x - \sigma_y}{2} \sin 2\theta + \tau_{xy} \cos 2\theta$$

and by setting $\theta = \theta + 90^\circ \Rightarrow$

$$\sigma_{y'} = \frac{\sigma_x + \sigma_y}{2} - \frac{\sigma_x - \sigma_y}{2} \cos 2\theta - \tau_{xy} \sin 2\theta$$



In-plane *principal stresses*

In-plane principal normal stresses can be obtained by:

$$\frac{d}{d\theta} \sigma_{x'} = \frac{d}{d\theta} \left(\frac{\sigma_x + \sigma_y}{2} + \frac{\sigma_x - \sigma_y}{2} \cos 2\theta + \tau_{xy} \sin 2\theta \right) = 0$$

resulting in an angle of:

$$\tan 2\theta_p = \frac{\tau_{xy}}{(\sigma_x - \sigma_y)/2}$$

which is substituted into transformation equation to lead to the **principal stresses (Max/Min)**:

$$\sigma_{1,2} \begin{matrix} (Max, Min) \end{matrix} = \frac{\sigma_x + \sigma_y}{2} \pm \sqrt{\left(\frac{\sigma_x - \sigma_y}{2} \right)^2 + \tau_{xy}^2}$$



Maximum and Minimum in-plane shear stress

Max/Min in-plane shear stresses can be obtained by:

$$\frac{d}{d\theta} \tau_{x'y'} = \frac{d}{d\theta} \left(-\frac{\sigma_x - \sigma_y}{2} \sin 2\theta + \tau_{xy} \cos 2\theta \right) = 0$$

resulting in an angle of: $\tan 2\theta_s = \frac{-(\sigma_x - \sigma_y)/2}{\tau_{xy}}$

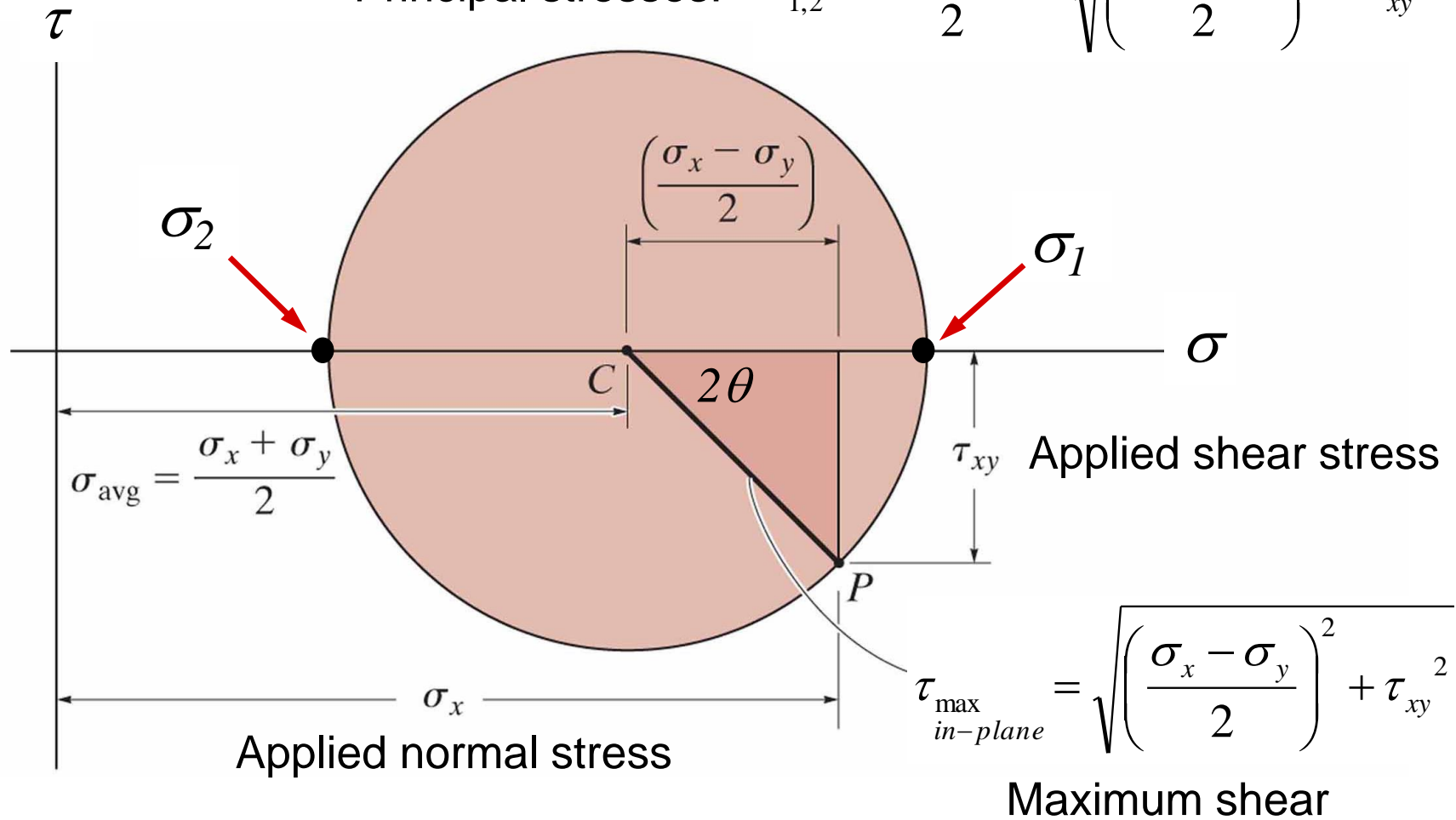
which is substituted into transformation equation to lead to the **maximum in-plane shear stress (Max/Min)**:

$$\tau_{\substack{\text{Max/Min} \\ \text{in-plane}}} = \pm \sqrt{\left(\frac{\sigma_x - \sigma_y}{2} \right)^2 + \tau_{xy}^2}$$



Mohr's circle (developed by Otto Mohr in 1882)

Principal stresses:
$$\sigma_{1,2} = \frac{\sigma_x + \sigma_y}{2} \pm \sqrt{\left(\frac{\sigma_x - \sigma_y}{2}\right)^2 + \tau_{xy}^2}$$



Principal and maximum shear stresses can be used to study failure of components

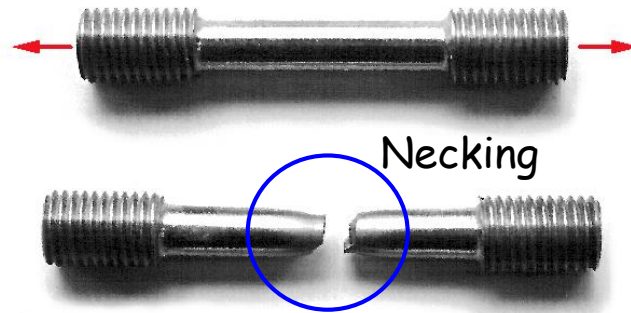


FIGURE 2-3

A Tensile Test Specimen of Mild, Ductile Steel After Fracture

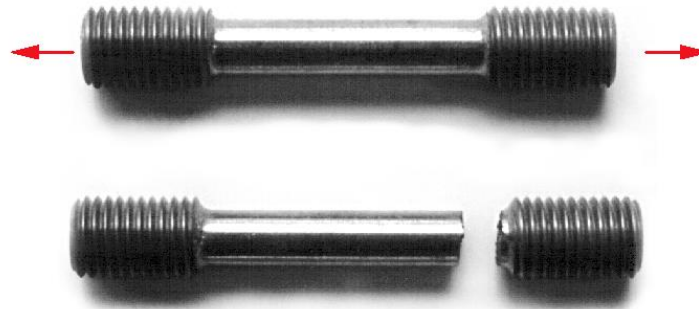


FIGURE 2-5

A Tensile Test Specimen of Brittle Cast Iron After Fracture

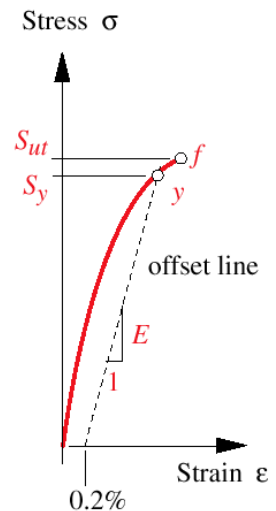


FIGURE 2-4

Stress-Strain Curve of a Brittle Material



Principal and maximum shear stresses can be used to study failure of components

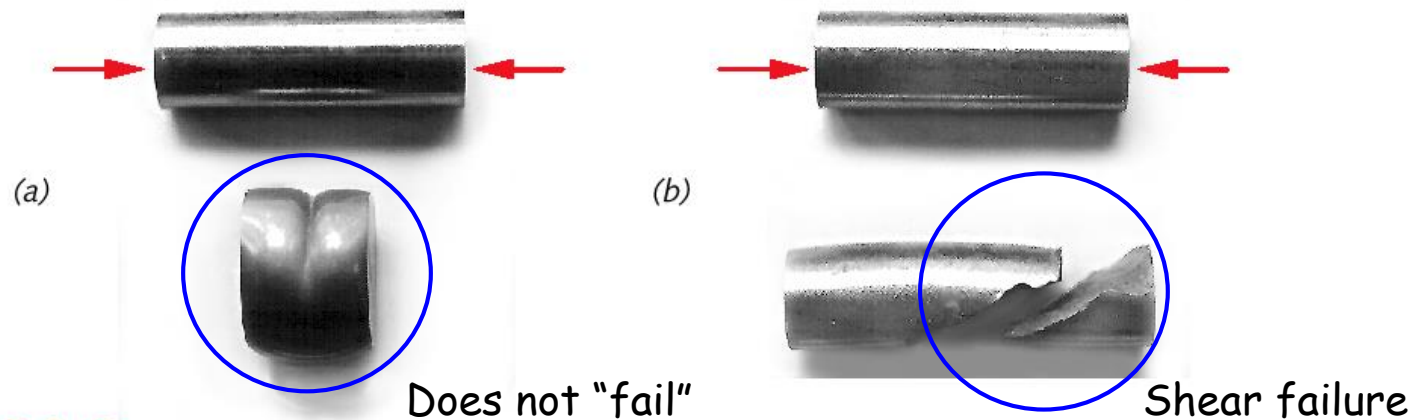


FIGURE 2-6

Compression Test Specimens After Failure (a) Ductile Steel (b) Brittle Cast Iron

Even materials: same behavior in tension and in compression.



Principal and maximum shear stresses can be used to study failure of components

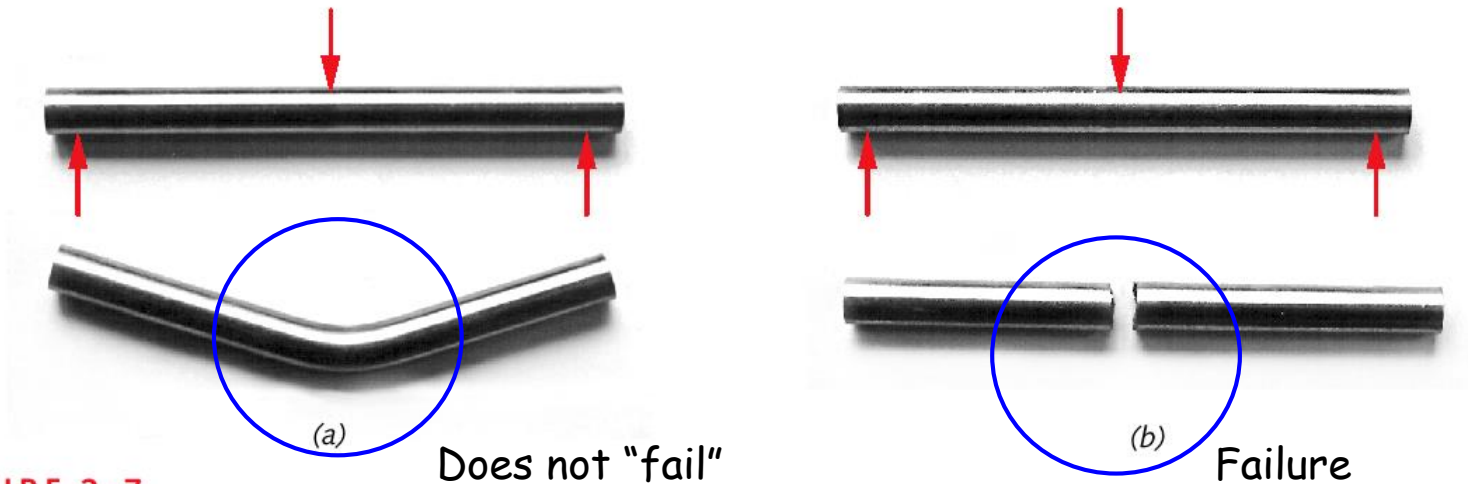
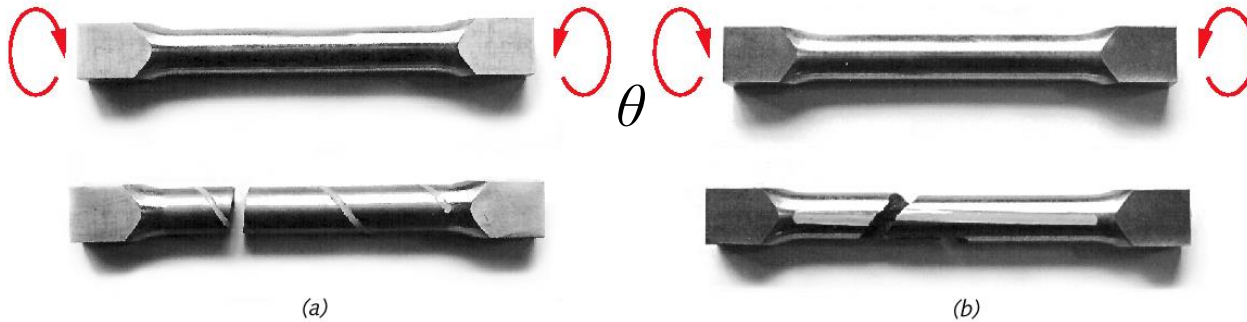


FIGURE 2-7

Bending Test Specimens After Failure (a) Ductile Steel (b) Brittle Cast Iron



Principal and maximum shear stresses can be used to study failure of components



Steels: $S_{us} = 0.80 S_{ut}$
 Other ductile
 mtl.: $S_{us} = 0.75 S_{ut}$
 Note: $S_{sy} = 0.58 S_y$

FIGURE 2-8

Torsion Test Specimens After Failure (a) Ductile Steel (b) Brittle Cast Iron

Stress-strain relation
 (torsion):
$$\tau = \frac{Gr\theta}{l_o}$$

Modulus of rigidity:

$$G = \frac{E}{2(1+\nu)}$$

Table 2-1

Poisson's Ratio ν

Material	ν
Aluminum	0.34
Copper	0.35
Iron	0.28
Steel	0.28
Magnesium	0.33
Titanium	0.34

Ultimate shear strength

(torsion):
$$S_{us} = \frac{T_{(break)}r}{J}$$

Not uniform stress
 distribution; (in some
 cases, thin-walled tubes
 are preferred for this
 test, **why?**)



Reading assignment

- Chapter 9 of textbook
- Review notes and text: ES2001, ES2501



Homework assignment

- As indicated on webpage of our course

