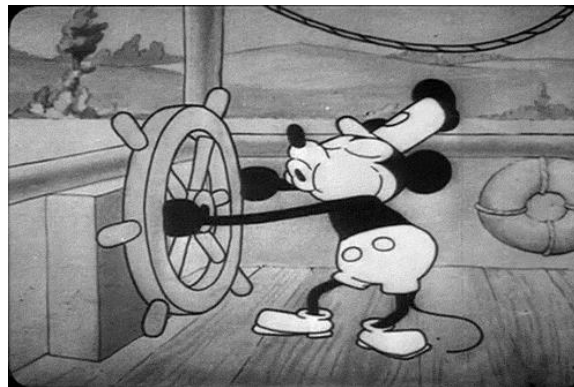


WORCESTER POLYTECHNIC INSTITUTE MECHANICAL ENGINEERING DEPARTMENT

STRESS ANALYSIS ES-2502, B'2025

We will get started soon...



06 November 2025



WORCESTER POLYTECHNIC INSTITUTE MECHANICAL ENGINEERING DEPARTMENT

STRESS ANALYSIS ES-2502, D'2020

Lecture 11:
Unit 6: tension/compression of slender
longitudinal bars: *statically indeterminate*

06 November 2025



General information

Instructor: Cosme Furlong

HL-152

(508) 831-5126

Email: cfurlong @ wpi.edu

<http://www.wpi.edu/~cfurlong/es2502.html>

Graduate Assistants:

→ Hamed Ghavami (TA)

Email: sghavami @ wpi.edu

→ Jay Patil (GA)

Email: jpatil1 @ wpi.edu

→ Mikayla Almeida (GA)

mpalmeida @ wpi.edu



Axial load

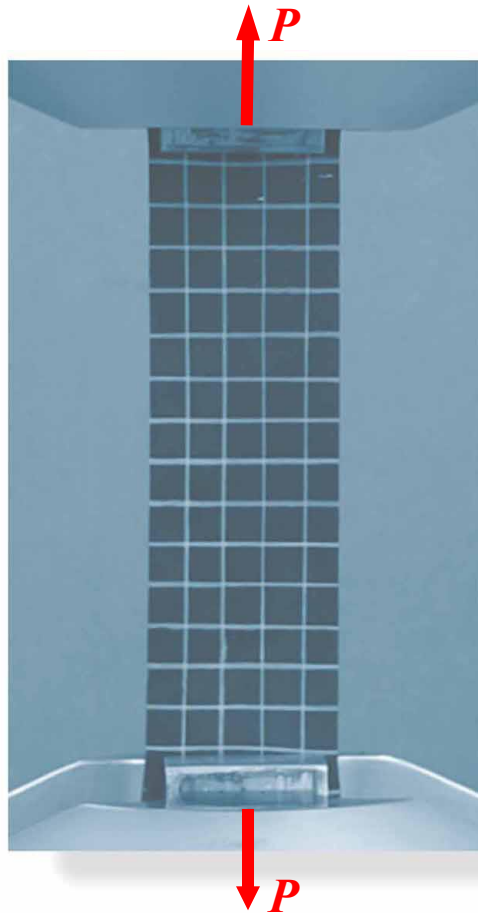


Figure: 04-01-UN-A

Notice how the lines on this rubber membrane distort after it is stretched. The localized distortions at the grips smooth out as stated by Saint-Venant's principle.

Note distortion lines: follow Saint-Venant's principle

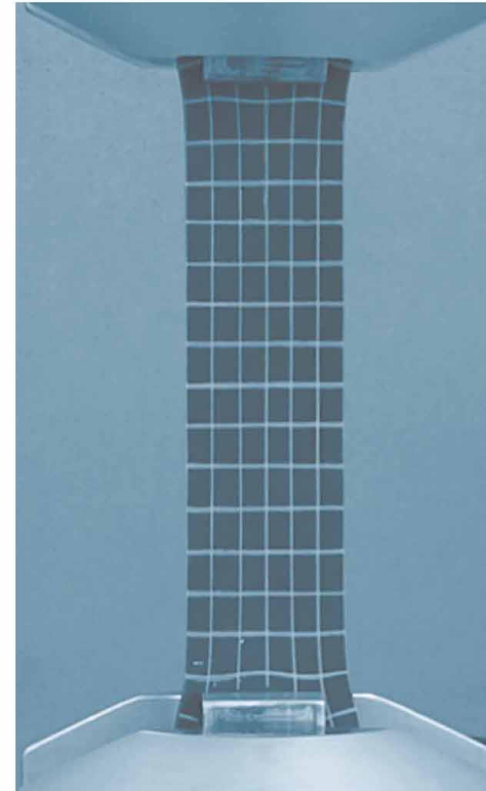


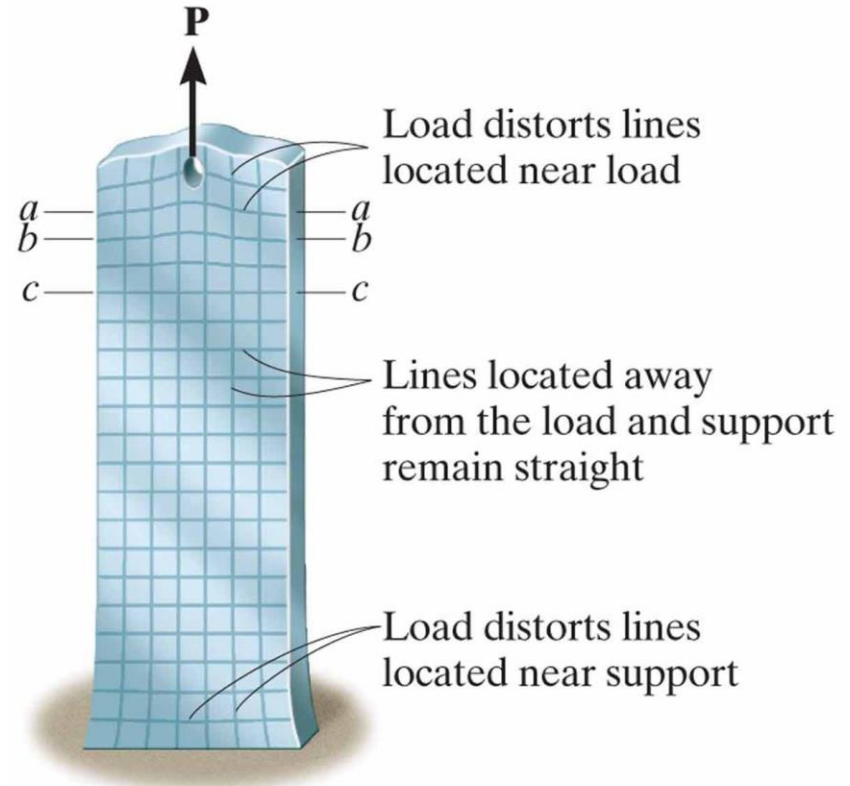
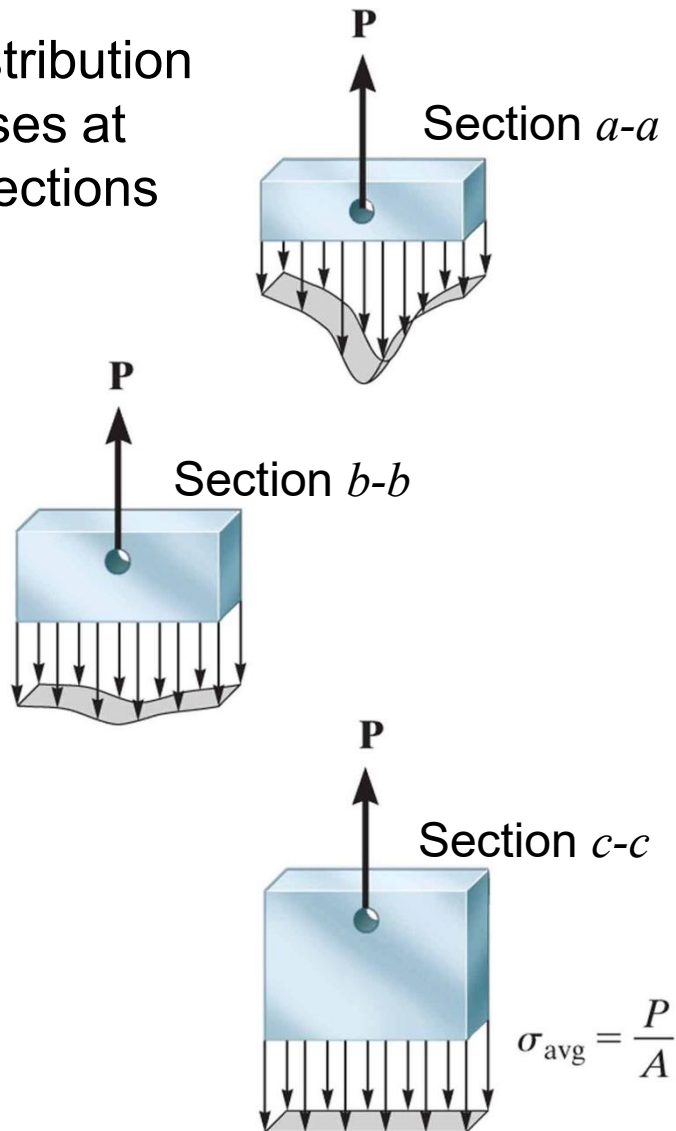
Figure: 04-01-UN-B

Notice how the lines on this rubber membrane distort after it is stretched. The localized distortions at the grips smooth out as stated by Saint-Venant's principle.

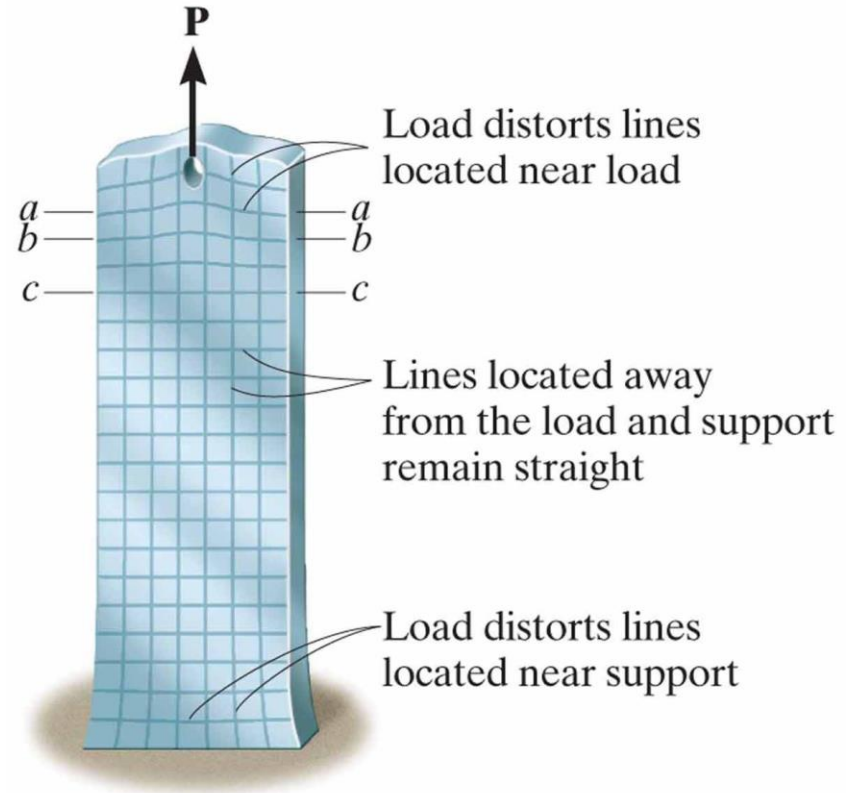
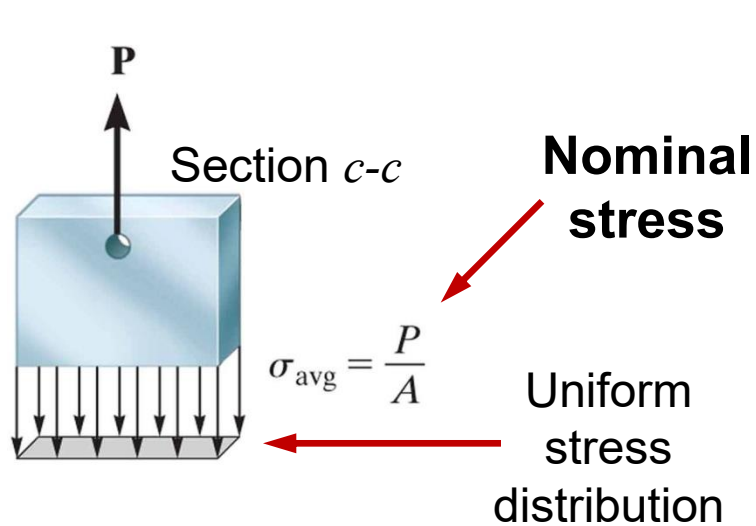


Axial load: Saint-Venant's principle

Internal distribution
of stresses at
various sections



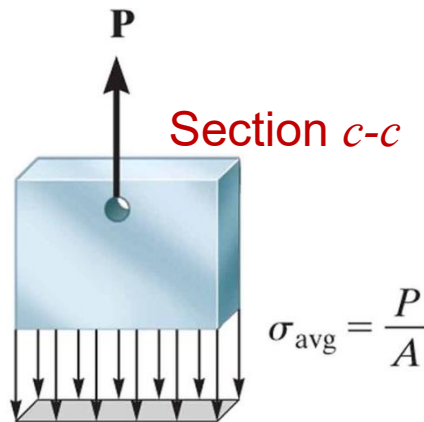
Axial load: Saint-Venant's principle



Axial load: Saint-Venant's principle

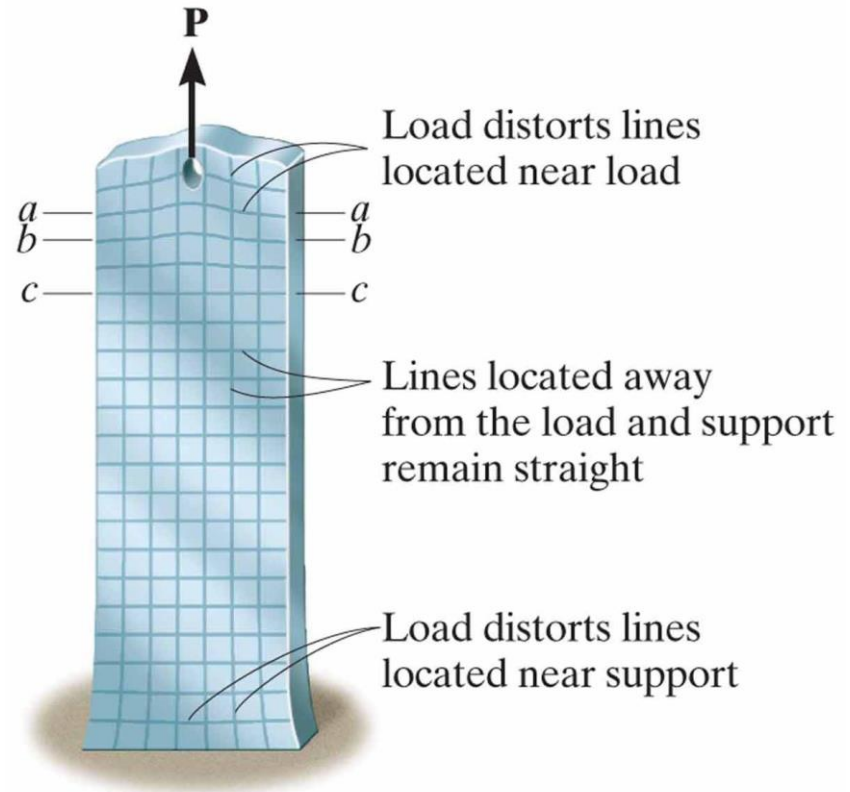
In your analyses, select locations (sections / points) located away from regions that are subjected to load application (to eliminate “end” effects)

Saint-Venant's principle: stresses and strains within a section will approach their nominal values as the section locates away from regions of load application

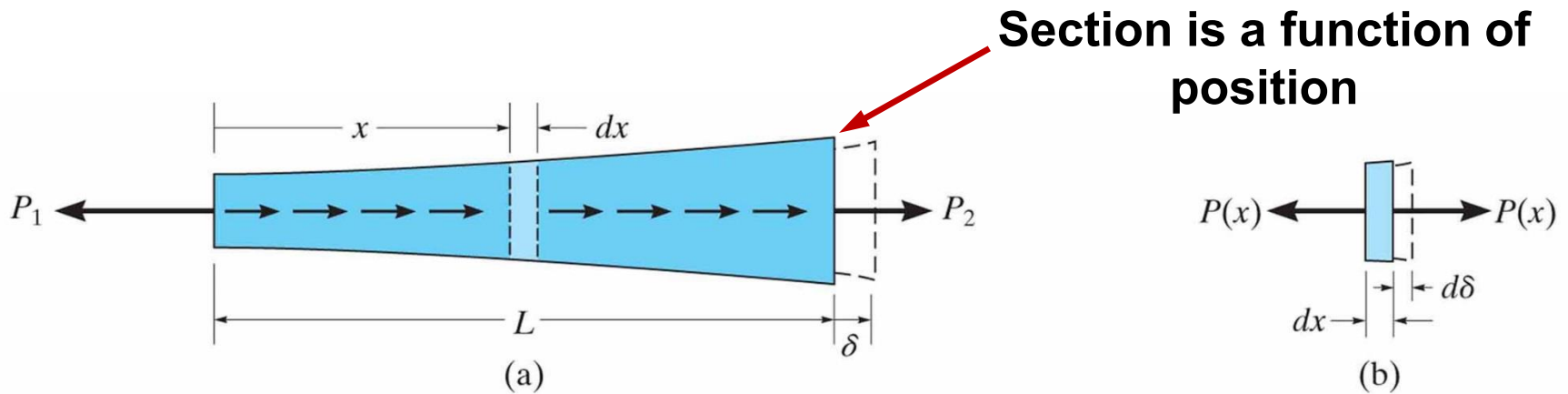


$$\sigma_{\text{avg}} = \frac{P}{A}$$

Nominal stress



Elastic deformation of an axially loaded member



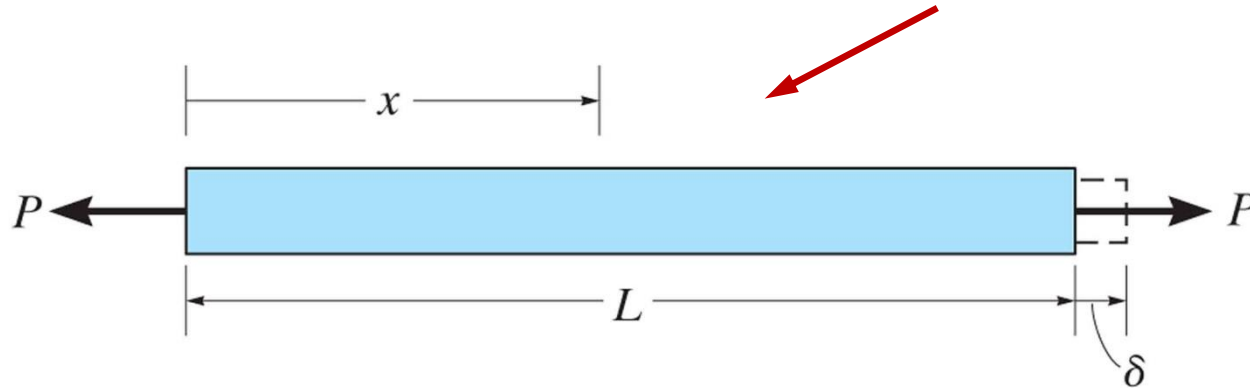
$$\sigma = \frac{P(x)}{A(x)} \quad \text{and} \quad \varepsilon = \frac{d\delta}{dx}$$

$$\text{Therefore, } d\delta = \frac{P(x) dx}{A(x) E} \quad \longrightarrow \quad \delta = \int_0^L \frac{P(x)}{A(x) E} dx$$



Elastic deformation of an axially loaded member

Constant load and cross-sectional area



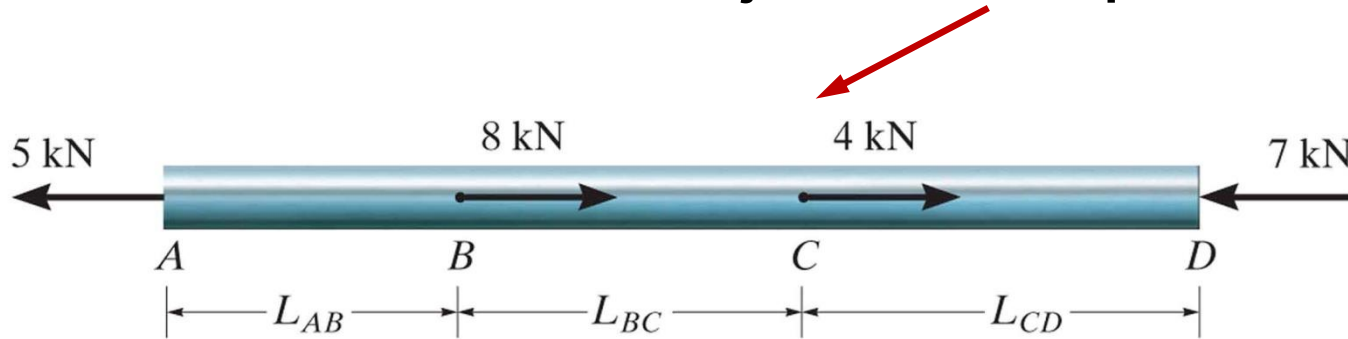
Elastic deformation:

$$\delta = \int_0^L \frac{P(x)}{A(x) E} dx = \frac{P}{A E} \int_0^L dx = \frac{P L}{A E}$$



Elastic deformation of an axially loaded member

Bar subjected to multiple axial loads



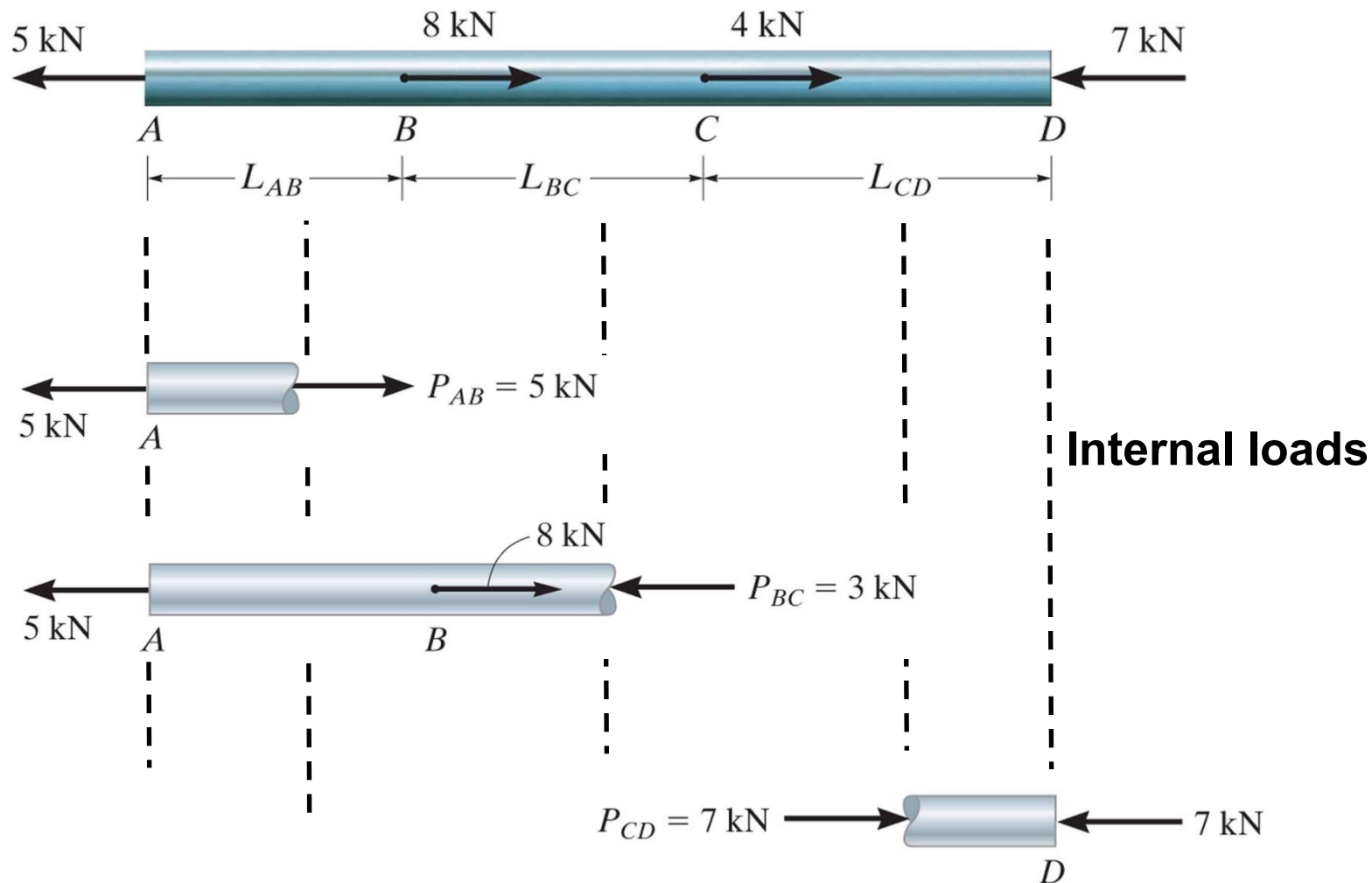
Elastic deformation:

$$\delta = \sum_i \left(\frac{P L}{A E} \right)_i$$



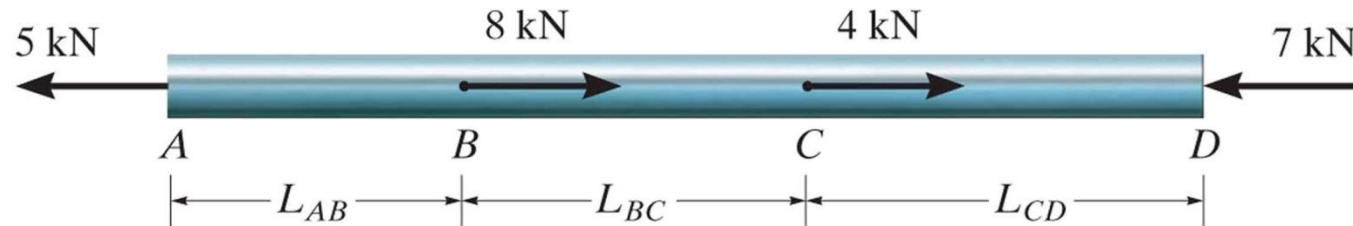
Elastic deformation of an axially loaded member

Procedure for analysis



Elastic deformation of an axially loaded member

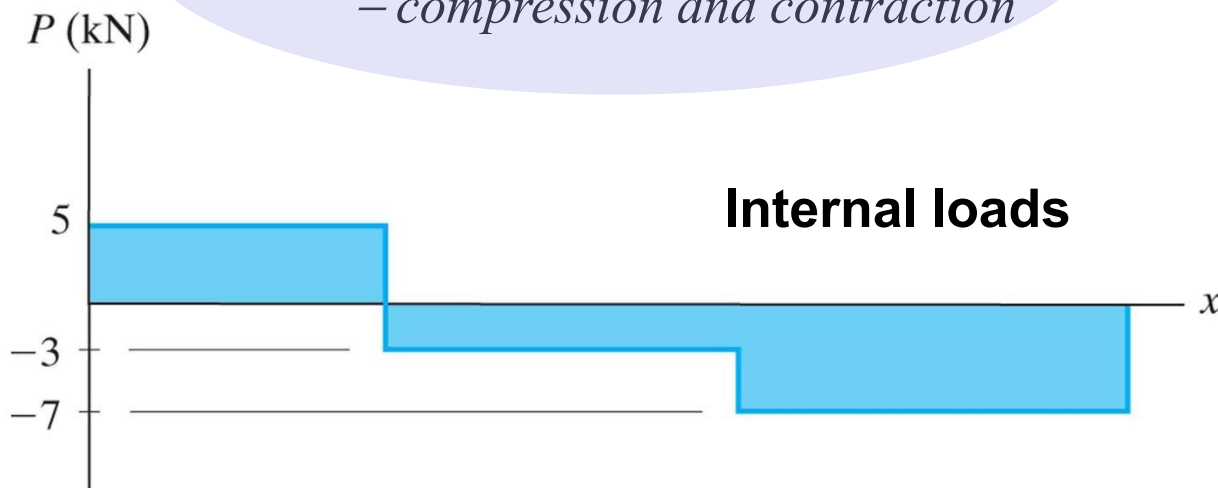
Procedure for analysis



Sign convention:

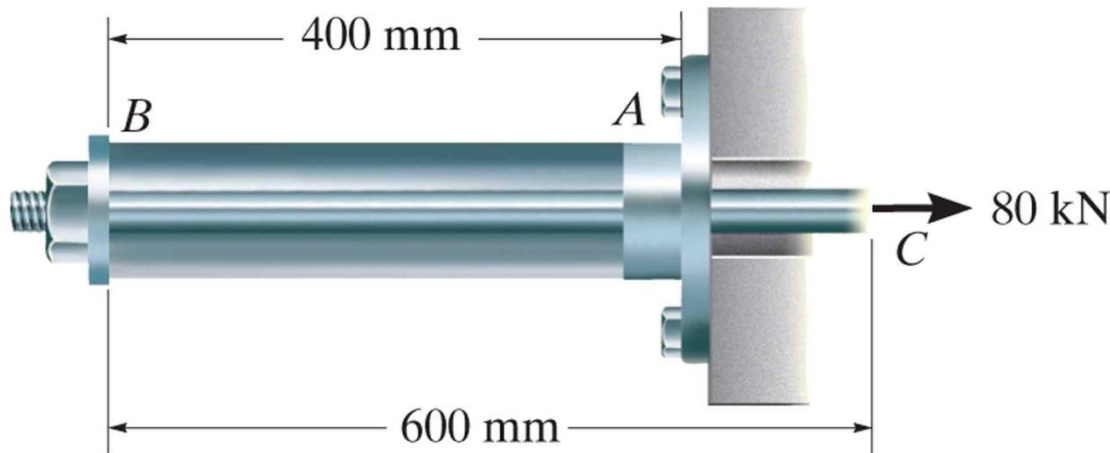
+ *tension and elongation*

– *compression and contraction*



Axial load: example D

The assembly shown consists of an aluminum tube AB having a cross sectional area of 400 mm^2 . A steel rod having a diameter of 10 mm is attached to a rigid collar and passes through the tube. If a tensile load of 80 kN is applied to the rod, determine the displacement of the end C of the rod. Elastic modules: $E_{\text{steel}} = 200 \text{ GPa}$ and $E_{\text{alum}} = 70 \text{ GPa}$



Approach:

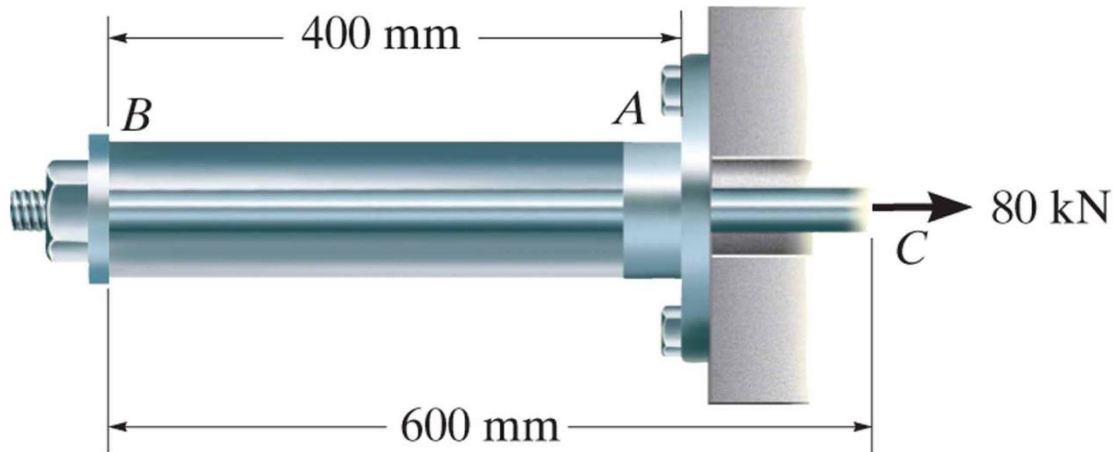
- 1) Determine internal loading
- 2) Compute displacement



Axial load: example D

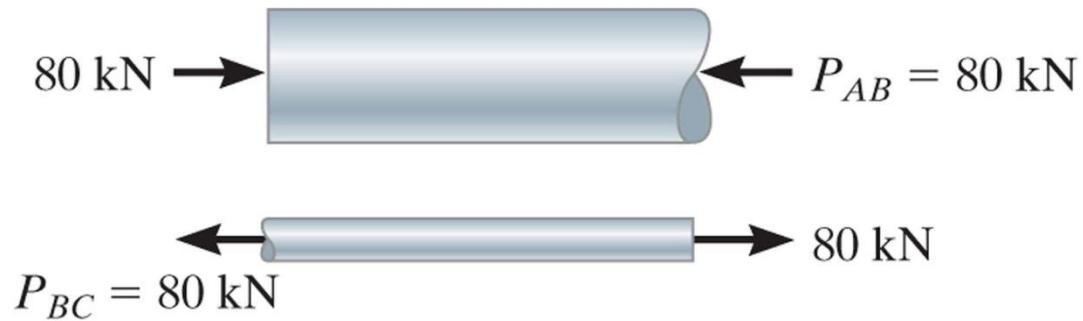
Displacement of C :

$$\delta_C = \delta_B + \delta_{C/B}$$

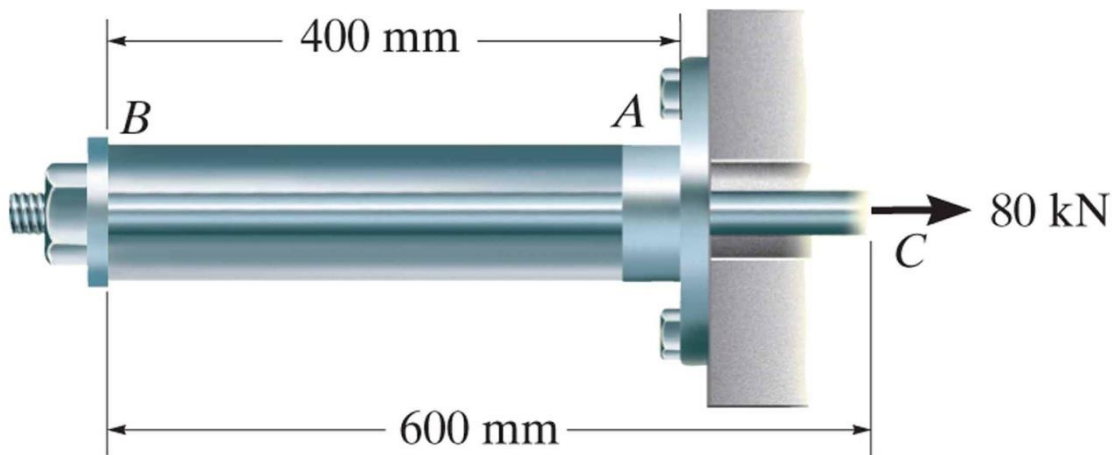


Axial load: example D

(1) Internal loading

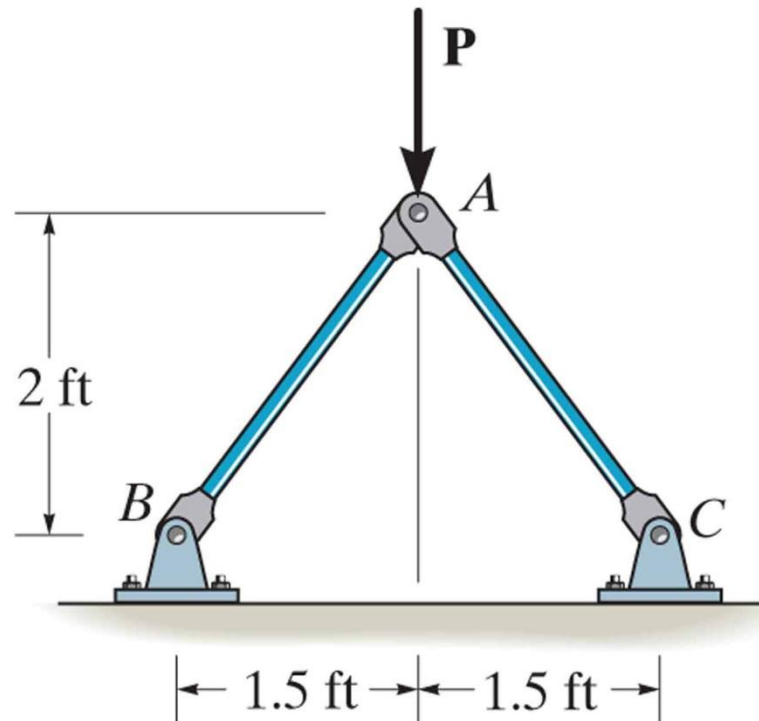


(2) → find displacement at C



Axial load: example E

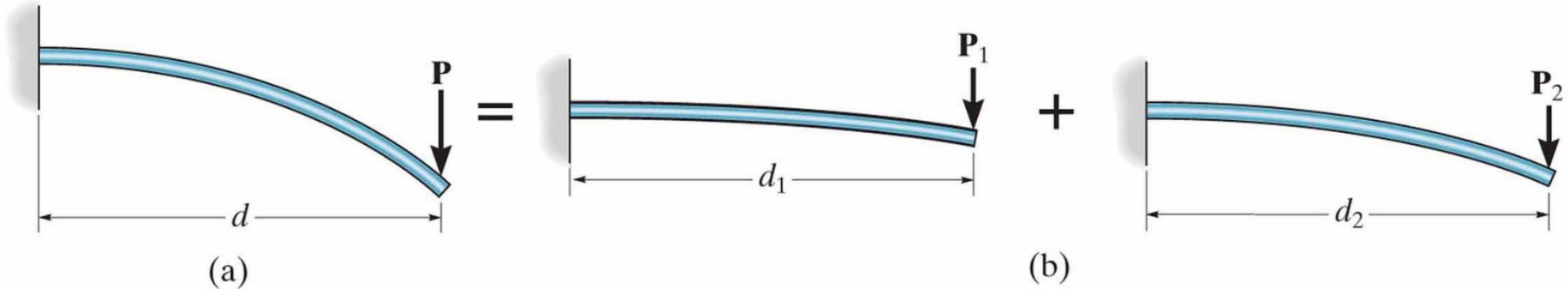
The linkage is made of two pin-connected A-36 steel members, each having a cross-sectional area of 1.50 in^2 . If a vertical force of P is applied to point A , determine its vertical displacement at A .



Principle of superposition

Applied when a component is subjected to complicated loading conditions → **break a complex problem into series of simple problems**

$$\mathbf{P} = \mathbf{P}_1 + \mathbf{P}_2$$



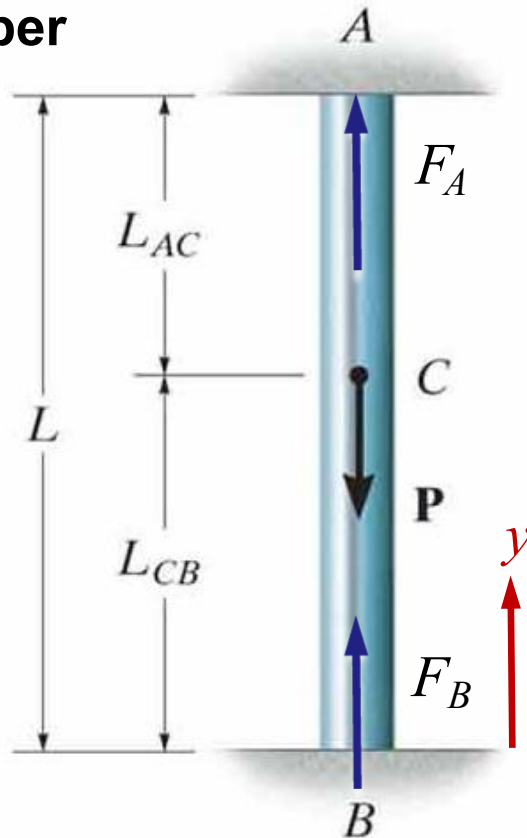
Can only be applied for:

- (a) small deformations;
- (b) deformations in the elastic (linear) range of the σ – ε diagram



Statically indeterminate axially loaded member

Axially loaded member



In this case, only one equilibrium equation:

$$+\uparrow \sum F_y = 0;$$

$$F_B + F_A - P = 0 \quad (1)$$

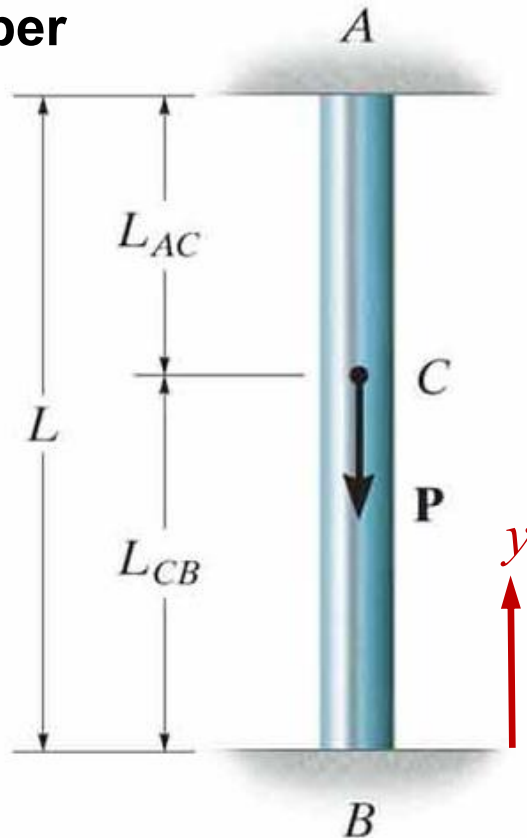
→ *Statically indeterminate problem*

Need additional equations!!



Statically indeterminate axially loaded member

Axially loaded member



Additional equations are obtained by applying:

Compatibility or kinematic equations

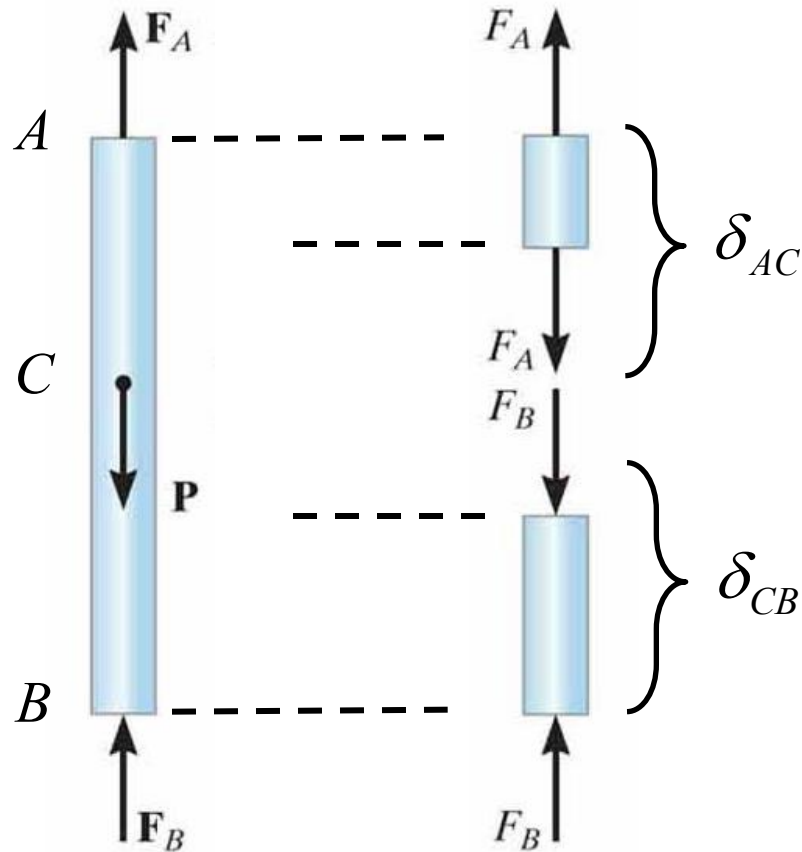


Load-displacement equations

$$\delta_{A/B} = 0$$



Statically indeterminate axially loaded member



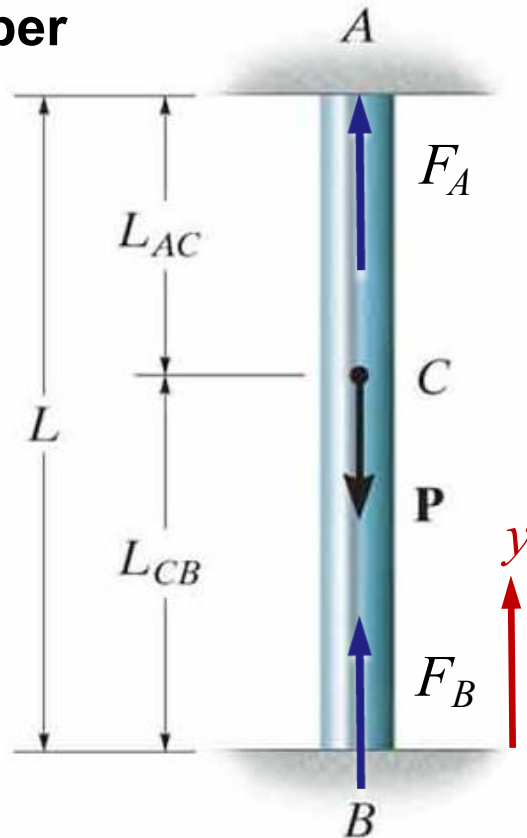
**Compatibility or
kinematic equations:**

$$\frac{F_A L_{AC}}{A E} - \frac{F_B L_{CB}}{A E} = 0 \quad (2)$$



Statically indeterminate axially loaded member

Axially loaded member



Forces are obtained by solving system of equations:

Equilibrium



$$F_B + F_A - P = 0 \quad (1)$$

$$\frac{F_A L_{AC}}{A E} - \frac{F_B L_{CB}}{A E} = 0 \quad (2)$$

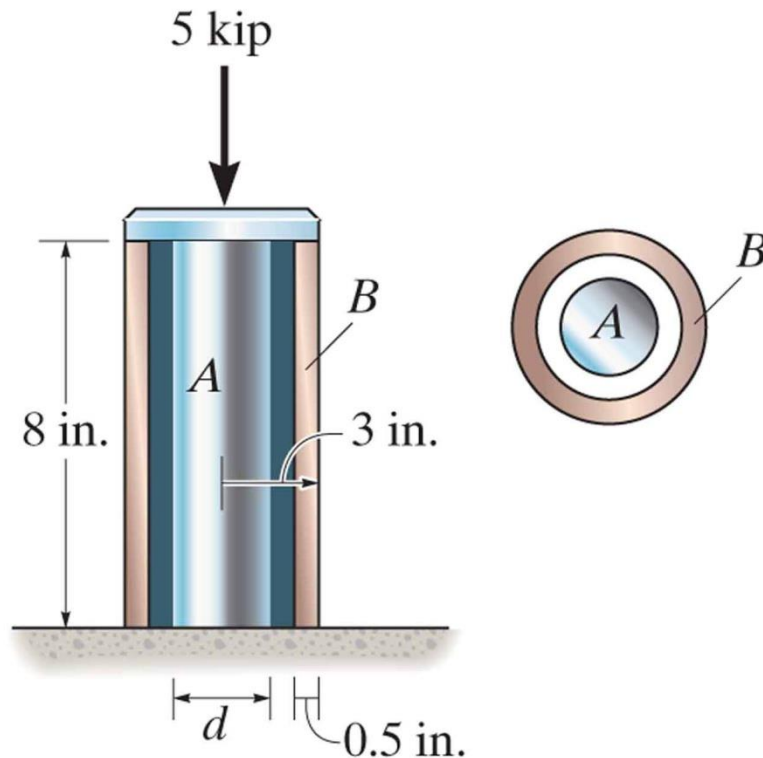


Compatibility



Axial load: example F

The 304 stainless steel post A has a diameter of $d = 2.0$ in and is surrounded by a red brass C83400 tube B . Both rest on the rigid surface. If a force of 5 kip is applied to the rigid cap, determine the average normal stress developed in the post and the tube.



Approach:

- 1) Apply equilibrium equations
- 2) Apply compatibility equations
- 3) Solve for stresses



Reading assignment

- Chapters 3 and 4 of textbook
- Review notes and text: ES2001, ES2501



Homework assignment

- As indicated on webpage of our course

